WILSON MILLS
ROAD
CHESTER TWP.

# LEVEL BOOK
# 373

# KEUFFEL & ESSER CO.

**DRAWING MATERIALS**
AND
**SURVEYING INSTRUMENTS.**
**NEW YORK.**

CHICAGO. ST. LOUIS. SAN FRANCISCO. MONTREAL.

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## TABLES FOR EXCAVATIONS AND EMBANKMENTS.



DISTANCES FROM CENTER OF ROAD VALUES FOR CROSS-SECTIONING.
ROADWAY 18 FEET WIDE. SIDE SLOPES 1 TO 1
FOR SINGLE TRACK EXCAVATION.



| | 0 | .1 | .2 | .3 | .4 | .5 | .6 | .7 | .8 | .9 | |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 0 | 9.0 | 9.1 | 9.2 | 9.3 | 9.4 | 9.5 | 9.6 | 9.7 | 9.8 | 9.9 | 0 |
| 1 | 10.0 | 10.1 | 10.2 | 10.3 | 10.4 | 10.5 | 10.6 | 10.7 | 10.8 | 10.9 | 1 |
| 2 | 11.0 | 11.1 | 11.2 | 11.3 | 11.4 | 11.5 | 11.6 | 11.7 | 11.8 | 11.9 | 2 |
| 3 | 12.0 | 12.1 | 12.2 | 12.3 | 12.4 | 12.5 | 12.6 | 12.7 | 12.8 | 12.9 | 3 |
| 4 | 13.0 | 13.1 | 13.2 | 13.3 | 13.4 | 13.5 | 13.6 | 13.7 | 13.8 | 13.9 | 4 |
| 5 | 14.0 | 14.1 | 14.2 | 14.3 | 14.4 | 14.5 | 14.6 | 14.7 | 14.8 | 14.9 | 5 |
| 6 | 15.0 | 15.1 | 15.2 | 15.3 | 15.4 | 15.5 | 15.6 | 15.7 | 15.8 | 15.9 | 6 |
| 7 | 16.0 | 16.1 | 16.2 | 16.3 | 16.4 | 16.5 | 16.6 | 16.7 | 16.8 | 16.9 | 7 |
| 8 | 17.0 | 17.1 | 17.2 | 17.3 | 17.4 | 17.5 | 17.6 | 17.7 | 17.8 | 17.9 | 8 |
| 9 | 18.0 | 18.1 | 18.2 | 18.3 | 18.4 | 18.5 | 18.6 | 18.7 | 18.8 | 18.9 | 9 |
| 10 | 19.0 | 19.1 | 19.2 | 19.3 | 19.4 | 19.5 | 19.6 | 19.7 | 19.8 | 19.9 | 10 |
| 11 | 20.0 | 20.1 | 20.2 | 20.3 | 20.4 | 20.5 | 20.6 | 20.7 | 20.8 | 20.9 | 11 |
| 12 | 21.0 | 21.1 | 21.2 | 21.3 | 21.4 | 21.5 | 21.6 | 21.7 | 21.8 | 21.9 | 12 |
| 13 | 22.0 | 22.1 | 22.2 | 22.3 | 22.4 | 22.5 | 22.6 | 22.7 | 22.8 | 22.9 | 13 |
| 14 | 23.0 | 23.1 | 23.2 | 23.3 | 23.4 | 23.5 | 23.6 | 23.7 | 23.8 | 23.9 | 14 |
| 15 | 24.0 | 24.1 | 24.2 | 24.3 | 24.4 | 24.5 | 24.6 | 24.7 | 24.8 | 24.9 | 15 |
| 16 | 25.0 | 25.1 | 25.2 | 25.3 | 25.4 | 25.5 | 25.6 | 25.7 | 25.8 | 25.9 | 16 |
| 17 | 26.0 | 26.1 | 26.2 | 26.3 | 26.4 | 26.5 | 26.6 | 26.7 | 26.8 | 26.9 | 17 |
| 18 | 27.0 | 27.1 | 27.2 | 27.3 | 27.4 | 27.5 | 27.6 | 27.7 | 27.8 | 27.9 | 18 |
| 19 | 28.0 | 28.1 | 28.2 | 28.3 | 28.4 | 28.5 | 28.6 | 28.7 | 28.8 | 28.9 | 19 |
| 20 | 29.0 | 29.1 | 29.2 | 29.3 | 29.4 | 29.5 | 29.6 | 29.7 | 29.8 | 29.9 | 20 |
| 21 | 30.0 | 30.1 | 30.2 | 30.3 | 30.4 | 30.5 | 30.6 | 30.7 | 30.8 | 30.9 | 21 |
| 22 | 31.0 | 31.1 | 31.2 | 31.3 | 31.4 | 31.5 | 31.6 | 31.7 | 31.8 | 31.9 | 22 |
| 23 | 32.0 | 32.1 | 32.2 | 32.3 | 32.4 | 32.5 | 32.6 | 32.7 | 32.8 | 32.9 | 23 |
| 24 | 33.0 | 33.1 | 33.2 | 33.3 | 33.4 | 33.5 | 33.6 | 33.7 | 33.8 | 33.9 | 24 |
| 25 | 34.0 | 34.1 | 34.2 | 34.3 | 34.4 | 34.5 | 34.6 | 34.7 | 34.8 | 34.9 | 25 |
| 26 | 35.0 | 35.1 | 35.2 | 35.3 | 35.4 | 35.5 | 35.6 | 35.7 | 35.8 | 35.9 | 26 |
| 27 | 36.0 | 36.1 | 36.2 | 36.3 | 36.4 | 36.5 | 36.6 | 36.7 | 36.8 | 36.9 | 27 |
| 28 | 37.0 | 37.1 | 37.2 | 37.3 | 37.4 | 37.5 | 37.6 | 37.7 | 37.8 | 37.9 | 28 |
| 29 | 38.0 | 38.1 | 38.2 | 38.3 | 38.4 | 38.5 | 38.6 | 38.7 | 38.8 | 38.9 | 29 |
| 30 | 39.0 | 39.1 | 39.2 | 39.3 | 39.4 | 39.5 | 39.6 | 39.7 | 39.8 | 39.9 | 30 |
| 31 | 40.0 | 40.1 | 40.2 | 40.3 | 40.4 | 40.5 | 40.6 | 40.7 | 40.8 | 40.9 | 31 |
| 32 | 41.0 | 41.1 | 41.2 | 41.3 | 41.4 | 41.5 | 41.6 | 41.7 | 41.8 | 41.9 | 32 |
| 33 | 42.0 | 42.1 | 42.2 | 42.3 | 42.4 | 42.5 | 42.6 | 42.7 | 42.8 | 42.9 | 33 |
| 34 | 43.0 | 43.1 | 43.2 | 43.3 | 43.4 | 43.5 | 43.6 | 43.7 | 43.8 | 43.9 | 34 |
| 35 | 44.0 | 44.1 | 44.2 | 44.3 | 44.4 | 44.5 | 44.6 | 44.7 | 44.8 | 44.9 | 35 |
| 36 | 45.0 | 45.1 | 45.2 | 45.3 | 45.4 | 45.5 | 45.6 | 45.7 | 45.8 | 45.9 | 36 |

Calculated by Julien A. Hall, M. Am. Soc. C. E.

Book #50

Wilson Mills Road No. 8
Chester Twp.
X-Sections

Corrected BM Elevations - page 37
Herzer pond (S. side Wilson Mills 1500 ft. W. of 306) - " 72
Wilson Mills Rd (Elev. N & S. Ditch's - Pg 74
Sta 189+87 to 203+00)

Return to the
County Surveyors Office
Court House
Chardon
Ohio

Cuyahoga Co. B.M. Station
24" Maple NE & Brigham Rd
& Co. Line Rd Elev 997.20
Cuy. Co. Datum

our elevation — 1072.36
Cuy. Co. Datum computes 1072.36 − 997.20 = 575.16

| | | Scotland to BM | | | Corrected Elevations |
|---|---|---|---|---|---|
| B.M.#6 | 5.13 | 1190.29 | | 1185.16 | |
| | 1.26 | 1180.69 | 10.86 | 1179.43 | |
| | 6.96 | 1185.63 | 2.02 | 1178.67 | |
| B.M.#7 = | Our BM#11 | | 6.92 | 1178.71 | 1177.78 |
| | 3.74 | 1189.00 | 0.37 | 1185.26 | |
| | 2.51 | 1178.80 | 12.71 | 1176.29 | |
| B.M.10 | | | 3.38 | 1175.42 | 1174.51 |
| | 0.00 | 1166.09 | 12.71 | 1166.09 | |
| | 2.39 | 1158.73 | 9.75 | 1156.34 | |
| B.M 9 | | | 3.17 | 1155.56 | 1154.61 |
| | 0.40 | 1146.52 | 12.61 | 1146.12 | |
| | 0.13 | 1134.18 | 12.47 | 1134.05 | |
| B.M 8 | | | 7.78 | 1126.40 | 1125.43 |
| | 0.75 | 1122.58 | 12.35 | 1121.83 | |
| | 1.56 | 1111.05 | 13.09 | 1109.49 | |
| B.M 7 | 1.61 | 1102.00 | 10.66 | 1100.39 | 1099.32 |
| | 2.54 | 1092.77 | 11.77 | 1090.23 | |
| B.M.6 | | | 2.23 | 1090.54 | 1089.46 |
| | 1.88 | 1082.03 | 12.62 | 1080.15 | |

Nov. 5, 1930 D. Parks
R. Hassel 2
T. Snyder

cold 30°

W. root 30" Oak Lt. sta. 56 on Scotland Station Rd. North

N. root 14" Maple Lt. sta 76+14 on Scotland Station Rd. = 60' Rt & sta 76+20

Sta. 70+80

S. root 12" Elm stump 700'± S of Cross Rd 20' Lt. of ℄

Sta. 65+00

W. root 12" Maple 30' Rt of ℄ 1400'± S of Cave Rd.

N. Root 12" Maple Rt of ℄ 28 sta. 59+40

S. root 18" Maple 25'± Lt. of ℄ sta. 48+15

fd Aug 58

W. root 35" Maple 30' Rt. sta. 41+30

| | | | | | Corrected Elevation | |
|---|---|---|---|---|---|---|
| | | 1082.03 | | | | |
| B.M 5 | 3.93 | 1080.15 | 5.81 | 1076.22 | 1075.11 | N.W. root 24" Maple 27' Rt sta. 32+90 |
| B.M 4 | 0.17 | 1075.13 | 4.85 | 1075.30 | 1074.21 | N. root 24" Maple 30' Rt sta. 26+30 |
| BM 3 | 2.39 | 1068.04 | 8.48 | 1066.65 | | → S & W inside 10" Hickory 30' Lt ℄ Sta 20+80 |
| B.M 2 | 5.07 | 1072.14 | 1.97 | 1067.07 | 1066.34 | S. root 24" Maple 60' Lt sta. 9+60 |
| | 4.93 | 1075.26 | 1.81 | 1070.33 | | |
| B.M 1 | | | 2.14 | 1073.12 | 1072.36 | S. root 18" Maple 36' Lt sta. 0+90 B.M. |

Nov. 6. 1930 D. Parks T. Snyder 4

Cloudy 35°

| | | | | | Corrected Elevation | |
|---|---|---|---|---|---|---|
| B.M.11 | 6.29 | 1185.00 | | 1178.71 | 1177.78 | N. root 15" Maple 60' Rt & Sta 76+20 |
| | 11.68 | 1196.11 | 0.57 | 1184.43 | | |
| | 5.97 | 1201.95 | 0.13 | 1195.98 | | |
| B.M.12 | 6.81 | 1201.95 | 6.81 | 1195.14 | 1194.24 | N. root 20" Apple 60' Rt. Sta 83+60 |
| | 12.39 | 1208.38 | 5.96 | 1195.99 | | |
| | 8.34 | 1216.43 | 0.29 | 1208.09 | | |
| B.M.13 | 6.01 | 1216.43 | 6.01 | 1210.42 | 1209.50 | N. root 38" Twin Elm 30' Rt. Sta 91+25 |
| | 11.48 | 1226.93 | 0.98 | 1215.45 | | |
| | 8.98 | 1235.26 | 0.65 | 1226.28 | | |
| B.M.14 | 1.88 | 1235.26 | 1.88 | 1233.38 | 1232.45 | N. root 48" Elm 50' Rt. Sta. 100+90 |
| | 12.69 | 1247.32 | 0.63 | 1234.63 | | |
| | 0.00 | 1236.08 | 11.24 | 1236.08 | | |
| | 2.36 | 1229.81 | 8.63 | 1227.45 | | |
| B.M.15 | 1.04 | 1225.99 | 4.86 | 1224.95 | 1223.77 | 2 spikes inside N. side 6" Maple 30' Rt. Sta 118+40 |
| | 0.25 | 1213.83 | 12.41 | 1213.58 | | |
| | 0.05 | 1202.36 | 11.52 | 1202.31 | | |
| | 0.20 | 1190.45 | 12.11 | 1190.25 | | |
| | 0.00 | 1181.53 | 8.92 | 1181.53 | | |
| B.M.16 | | | 5.89 | 1175.64 | 1174.37 | N. root 18" Elm 25' Rt. Sta 134+01 |

| | | | | | Corrected Elevation | |
|---|---|---|---|---|---|---|
| B.M. 16 | 4.60 | 1180.24 | | 1175.64 | 1174.37 | N. root 12" Elm 23' Rt. Sta 134+01 |
| | 4.50 | 1183.27 | 1.47 | 1178.77 | | |
| | 6.19 | 1176.42 | 13.04 | 1170.23 | | |
| B.M. 17 | 6.21 | 1176.92 | 6.21 | 1170.21 | 1168.92 | 2 Horizontal spike N.W. side 24" Ash 45° Rt E Rt. Sta 145+0 |
| | 4.14 | 1179.89 | 0.67 | 1175.75 | | |
| B.M 18 | | | 3.89 | 1176.00 | 1174.73 | N.W. root 14" Maple R Sta. 162+10 Chillicothe R. |
| | | | | 1174.73 | record. | From Chillicothe Plans = 300' Lt & Sta 145+50, Wilson Mills Rd |

Check levels on Chillicothe Rd

Nov. 7, 1930 D. Parks
T. Snyder

South to Govt BM. at Chesterland

Clear 40° 48°

| | | | | | | |
|---|---|---|---|---|---|---|
| B. M 18 | 4.04 | 1178.77 | | 1174.73 | | Staple in N.W. root 14" Maple Chillicothe Rd |
| | 0.41 | 1166.31 | 12.87 | 1165.90 | | = 300' Lt & Sta 145+52 Wilson Mills Rd |
| | 11.87 | 1176.85 | 1.33 | 1164.98 | | |
| | 13.07 | 1189.57 | 0.35 | 1176.50 | | |
| | 10.55 | 1198.65 | 1.47 | 1188.10 | | |
| B. M | 11.19 | 1207.86 | 1.98 | 1196.67 | 1196.66 | Staple in W. root 30" Elm |
| | 12.37 | 1220.07 | 0.16 | 1207.70 | | |
| | 11.81 | 1231.61 | 0.27 | 1219.80 | | |
| | 12.18 | 1242.96 | 0.83 | 1230.78 | | |
| | 11.67 | 1254.14 | 0.49 | 1242.47 | | |
| | 12.58 | 1266.31 | 0.41 | 1253.73 | | |
| | 3.66 | 1269.75 | 0.22 | 1266.09 | | |
| | 1.06 | 1257.83 | 12.98 | 1256.77 | | |
| | 0.00 | 1245.94 | 11.89 | 1245.94 | | |
| | 1.60 | 1234.65 | 12.89 | 1233.05 | | |
| | 3.86 | 1225.79 | 12.72 | 1221.93 | | |
| B. M | | | 8.97 | 1216.82 | 1216.88 | Govt BM. Cottrells store Chesterland |

Nov. 7, 1930 D. Parks
T. Snyder 7

Clear 40°

| | | | | | Corrected Elev. | |
|---|---|---|---|---|---|---|
| B.M.18 | 3.42 | 1178.15 | | 1174.73 | | Staple N.W. root 14" Maple = 300' Lt & Sta 145+50 |
| | 0.07 | 1166.01 | 12.21 | 1165.94 | | |
| | 1.00 | 1155.97 | 11.04 | 1154.97 | | |
| B.M.19 | | | 4.49 | 1151.48 | 1151.45 | Spike N. root 24" Maple 24' Rt. Sta. 150+01 |
| | 1.50 | 1146.00 | 11.47 | 1144.50 | | |
| | 0.27 | 1133.32 | 12.95 | 1133.05 | | |
| | 8.05 | 1134.40 | 7.97 | 1125.35 | | |
| B.M.20 | | | 6.77 | 1127.63 | 1127.53 | Bent Spike N. root 20" Maple 25' Rt. Sta. 158+70 |
| | 12.31 | 1146.32 | 0.39 | 1134.01 | | |
| | 8.49 | 1154.62 | 0.19 | 1146.13 | | |
| | 2.66 | 1147.52 | 9.76 | 1144.86 | | |
| B.M.21 | | | 3.67 | 1143.85 | 1143.76 | Spike S. root 24" Elm 25' Lt. Sta. 168+40 |
| | 2.09 | 1139.13 | 10.48 | 1137.04 | | |
| | 2.73 | 1130.11 | 11.75 | 1127.38 | | |
| B.M.22 | | | 4.46 | 1125.65 | 1125.55 | 20' N of & 30' W of Corner of House Spike N. root 20" Maple 35' Rt. Sta. 177+30 |
| | 0.85 | 1118.44 | 12.52 | 1117.59 | | |
| | 3.27 | 1108.89 | 12.82 | 1105.62 | | |
| B.M.23 | | | 0.55 | 1108.34 | 1108.21 | Spike S.E. root 24" Apple 60' Lt. Sta. 183+30 |
| | 0.64 | 1097.11 | 12.42 | 1096.47 | | |

| | | | | | corrected Elev | |
|---|---|---|---|---|---|---|
| | | 1097.11 | | | | |
| | 3.14 | 1090.21 | 10.04 | 1087.07 | | |
| B.M. #24 | | | 5.06 | 1085.15 | 1084.94 | X-N.E. cor. N. Headwall Sta 189+90 12'Lt |

# Cross Sections

| | | | | |
|---|---|---|---|---|
| B.M.1 | 2.80 | 1075.16 | | 107236 |
| 0+00 | | | 7.6 | 67.6 |
| 0-50 | | | 9.5 | 65.7 |
| -100 | | | 10.1 | 65.1 |
| -150 | | | 10.6 | 64.6 |
| -200 | | | 11.3 | 639 |
| -250 | | | 11.8 | 63.4 |
| -300 | | | 12.2 | 63.0 |
| 0-25 | Vit. Pipe culvert | | 8.5 | 66.7 |
| 0+00 | | | 7.4 | 67.6 |
| 0+25 | Cast iron pipe | | 6.6 | 68.6 |
| 1 | | | 5.0 | 70.2 |
| 2 | | | 5.5 | 69.7 |
| 2+65 | | | 5.4 | 69.8 V |

Nov. 8, 1930
D. Parks T. Snyder-R.
R. Hassel F. Gray -

Spike in 18" Maple 30 Lt. Sta. 0+90

30 26 25 21 19 17 25 31 T.H. 34 T.H.
6.7 10.5 9.6 7.7 8.8 8.9 8.3 8.5 8.7 8.5 8.5 8.2 10.4 11.2
F.L. T.O T.H

75 100 150 T.H. 200 T.H.
11.3 11.6 12.2 13.5

200 150 100 50 50 100 150 200
0.1 2.2 5.7 5.2 7.6 10.0 10.6 11.4 12.0

30 14 12 12 Top 0. 7 11.5 Top 0 F.L. 50 100 150 200
4.4 5.1 6.6 7.5 6.9 6.5 6.6 7.1 7.6 8.7 10.9 11.9 12.7 13.6
67.7 66.5

30 11 7 4.5 10.5 12 90
2.7 4.2 6.1 5.0 5.1 6.1 5.5 5.6

30 10.5 8 4 9 11 30
3.3 4.5 6.2 5.5 5.7 6.3 5.6 6.7

60 11 10 7 7 8 11 50 100
6.1 7.2 5.8 5.4 6.2 7.4 8.4 9.2 10 10.5 V
F.L. P.P. P.L. 6 200
6.0 12.8

| | | | | |
|---|---|---|---|---|
| | | 1075.16 | | |
| 3 | | | 5.7 | 69.5 |
| | 2.51 | 1071.35 | 6.32 | 1068.84 |
| 4 | | | 2.7 | 68.7 |
| 5 | | | 5.3 | 66.1 |
| 5+25 | V.S.P. | culvert | 5.3 | 66.1 |
| 6 | | | 4.8 | 66.6 |
| 6+75 | | | 2.9 | 68.5 |
| 7 | | | 3.5 | 67.9 |
| | 3.36 | 1068.10 | 5.61 | 1065.74 |
| 8 | | | 3.5 | 65.6 |
| 9 | | | 6.6 | 62.5 |
| 9+23 | | | 7.0 | 62.1 |

30/7.7 16.5/4.9 7/6.4 —/5.7 8/6.6 9.5/5.5 30/5.8

30/0.8 20/4.8 11/1.8 8/4.5 6/3.5 —/2.7 4.5/3.0 8/3.8 11/1.5 30/1.7

30/5.8 14/5.8 10/6.2 8/5.6 —/5.3 6/5.6 8/6.2 9/5.9 30/6.4

100/5.5 30/6.6 —/7.3 7/5.6 —/5.3 8/5.8 8/7.1 8/8.2 50/9.4 100/10.9
F.L. 1064.1 & T.O. F.L. 1063.2

30/2.9 11/3.9 9/5.8 —/4.8 6/5.3 8/6.2 12.5/3.1 30/3.4

30/1.9 11/2.9 10/4.1 —/2.9 6/3.6 9/4.5 11/2.2 30/3.0

30/2.1 13/3.3 10.5/5.0 —/3.5 5/4.2 8.5/5.1 11/2.7 30/3.2

30/1.9 14/4.0 11/5.3 —/3.5 5.5/4.2 8/5.3 9.5/4.2 30/4.8

30/5.5 25/5.5 18/7.1 10/7.0 9/7.5 —/6.6 6.5/7.1 8.5/7.7 10/7.3 30/7.5

50/7.5 30/8.0 11/8.7 8.1/F.L. 1060.4 10/7.8 —/7.0 6/7.5 9/8.5 & 9/8.8 T.O. 9/9.0 F.L. 1060.1 30/8.9 50/10 100/14.2

| | | | | | |
|---|---|---|---|---|---|
| | | 1069.10 | | | |
| B.M. 2 | 2.64 | 1068.98 | 2.64 | 1066.46 | 1066.34 |
| 10 | | | 5.4 | 63.4 | |
| 11 | | | 5.1 | 63.9 | |
| | 4.44 | 1068.50 | 4.92 | 1064.06 | |
| 12 | | | 5.3 | 63.2 | |
| 12+70 ± | 1X1 stone box | | 4.9 | 63.6 | |
| 13 | | | 5.3 | 63.2 | |
| 14 | | | 4.7 | 63.8 | |
| 15 | | | 4.3 | 64.2 | |
| 16 | | | 4.3 | 64.2 | |
| | 2.91 | 1069.36 | 2.05 | 1066.45 | |
| 17 | | | 3.9 | 65.5 | |

Spike in 24" Maple 60' Lt ℄ Sta 9+60

30/3.1 24/3.5 23/4.7 9/6.3 —/5.4 7/6.2 13/4.6 30/5.4

30/4.5 20/4.6 11/5.9 10/4.2 7/5.1 —/5.1 8/5.7 18/5.5 30/6.6

30/4.2 11/5.5 9/4.7 7/5.6 —/5.3 10/6.0 12/5.9 30/7.1

30/4.5 30/5.9 St. 047 Pitch 1½ 30/6.1 9/4.7 Dim ℄ F.L. 1061.8 —/5.7 T.D. 8/5.0 —/4.9 6.5/5.3 7/5.9 T.O. 6.9 F.L. 1061.6 25/7.1 50/8.4 100/10.0

30/5.0 13/5.5 10/4.2 9/5.7 —/5.3 8/6.0 9/5.8 30/6.2

30/4.6 13/5.4 11/6.3 —/4.7 7/6.0 8/5.9 30/6.0

30/4.5 12/5.2 10/6.0 8/5.2 —/4.3 9/5.9 10/5.5 30/6.0

30/4.5 13/4.5 11/5.2 9/4.7 —/4.3 8/5.3 9/4.9 30/4.5

30/4.0 11/4.4 7/5.3 —/3.9 8/4.9 9/4.7 30/4.0

| | | | | |
|---|---|---|---|---|
| | | 1069.36 | | |
| 18 | | | 3.5 | 65.9 |
| 19 | | | 4.2 | 65.2 |
| 19+46 | 2'x1½' | Stone box | 3.8 | 65.6 |
| 20 | | | 4.0 | 65.4 |
| 21 | | | 3.1 | 66.3 |
| 22 | | | 1.2 | 68.2 |
| | 6.27 | 107538 | 0.25 | 1069.11 |
| 23 | | | 5.9 | 69.5 |
| 24 | | | 5.5 | 69.9 |
| 25 | | | 4.1 | 71.3 |
| 26 | | | 2.9 | 72.5 |

30/3,9 12/4,3 10/4,8 —/3,5 8/4,6 9/4,3 30/4,1

30/4,1 12/4,1 11/5,1 —/4,2 8/4,8 11/4,4 30/4,7

30/4,4 20/4,9 10/5,9-7,6 8/4,0 —/3,8 4/3,7 6/4,7 6/6,1 14/6,4 14/6,0 14/5,3 100/6,2 200/7,5
St. aux F.L. 7.0 — 7.0 F.L F.L T.P. G. Drain Pipe G
10635 10630

30/4,0 12/4,7 10/5,3 8/4,7 —/4,0 10/4,9 11/4,4 30/4,6

30/3,4 12/3,6 9/4,3 8/3,6 —/3,1 10/4,4 12/3,2 30/2,5

30/0.1 19/0,1 10/2,9 7/1,8 8/1,21,7 10/2,4 12/1,6 30/1,6

30/7,1 11/7,0 9/7,5 —/5,9 10/7,4 11/6,1 30/6,7

30/5,3 12/5,9 9/4,6 —/5,5 10/6,5 12/6,0 30/5,1

30-25/3,5 10/5,5 —/4,1 12/5,5 15/3,8 30/3,6
7/3,6

30/3,4 12/4,0 10/4,3 —/2,9 10/4,4 13/3,4 30/3,4

| | | | | | |
|---|---|---|---|---|---|
| | | 1075.38 | | | |
| B.M.#4 | | | 1.13 | 1074.25 | 1074.21 |
| | 4.22 | 1078.43 | | | |
| 27 | | | 5.7 | 72.7 | |
| 28 | | | 4.9 | 73.5 | |
| 29 | | | 4.4 | 74.0 | |
| 30 | | | 3.4 | 75.0 | |
| 31 | | | | 74.7 | |
| T.P | 5.68 | 1079.76 | 4.35 | 1074.08 | |
| 32 | | | 5.4 | 74.4 | |
| B.M.5 | 4.65 | 1079.76 | 4.65 | 1075.11 | 1075.11 |
| 33 | | | 5.9 | 73.9 | |
| 33+60 | 12" V.S.P | | 5.7 | 74.1 | |
| 34 | | | 5.8 | 74.0 | |

30/6.1 13/6.5 12/7.0 10/6.4 —/5.7 9/6.9 10/6.5 30/6.4

30/4.8 14/5.7 12/6.3 10/5.7 —/7.9 8/6.2 9/5.6 30/5.3

30/4.0 18/4.8 13/5.3 9/4.7 —/4.4 — 30/4.4

30/3.0 14/3.7 12/4.6 9/3.9 —/3.4 8/4.8 12/3.7 30/3.5

3.9/30 12/4.2 11/5.2 —/3.7 8/5.1 11/4.5 30/6.4

30/5.4 12/6.5 11/7.3 5.4 9/7.2 10/6.7 30/6.9

30/5.9 14/6.4 12/7.3 —/5.9 7/7.6 10/6.8 15/6.9 20/6.0 30/6.2

150/6.6 100/7.2 30/7.0 10/7.3 FL 10/6.5 7.0 7/5.7 —/5.7 8/5.9 9/6.4 T.P 9/7.4 FL 30/8.0 100/8.7

1072.5 1072.4 200/9.7

30/6.3 14/6.1 12/6.9 9/6.0 —/5.8 6/6.4 7/6.3 14/6.9 21/5.4 30/5.3

## Check Bench

| | | | | | |
|---|---|---|---|---|---|
| B.M. #3 | 1.13 | 1075.16 | | 1074.03 | |
| | 0.16 | 1069.05 | 6.27 | 1068.89 | |
| | 2.42 | 1068.65 | 2.82 | 1066.23 | |
| B.M. #2 | 3.86 | 1069.66 | 2.52 | 1066.13 | 1065.80 |
| | 5.64 | 1073.86 | 1.44 | 1068.22 | |
| B.M. #1 | | | 2.08 | 1071.78 | 1071.85 |

| | | | | | |
|---|---|---|---|---|---|
| | | 1079.60 | | | |
| | | 1072.76 | | | |
| 35 | | | 4.6 | 75.2 | |
| T.P | 7.79 | 1083.93 | 3.62 | 1076.14 | |
| 36 | | | 7.7 | 76.2 | |
| 37 | | | 7.1 | 76.8 | |
| 38 | | | 6.0 | 77.9 | |
| 39 | | | 4.3 | 79.6 | |
| 40 | | | 1.4 | 82.5 | |
| T.P | 9.77 | 1093.12 | 0.58 | 1083.35 | |
| 41 | | | 7.1 | 86.0 | |
| B.M 6 | | | 3.66 | 1089.46 | 1089.46 |



30/5.2 13/5.5 11/6.3 9/5.4 —/4.6 8/6.1 10/5.6 18/3.7 30/3.5

30/6.1 12/8.7 10.5/9.7 9/8.7 —/7.7 8/8.5 10.5/9.5 11/8.9 16/8.7 30/8.8

30/7.5 11/8.3 9/8.8 6/7.7 —/7.1 11/8.0 13/7.8 30/8.2

30/6.3 11/7.0 9/7.6 —/6.0 7/6.6 10/7.3 12/6.6 30/7.0

30/4.2 12/5.0 9/6.0 6/4.9 —/4.3 7.5/4.8 10.5/5.8 12/5.0 30/4.2

30/0.5 14/0.8 10/3.3 7/2.4 —/1.4 7.5/2.0 11/3.2 14/1.4 30/0.8

30/5.7 15/6.8 10/9.2 8/8.0 —/7.1 10/8.8 13/6.4 30/5.7

Spike, N.W. Root 24" Maple, Right Sta 41+50

Stopped, Nov. 8, 1930. 3 o'clock

Nov. 14, 1930
D. Parks,
R. Hasse
T. Snyder

| | | | | |
|---|---|---|---|---|
| B.M. 6 | 6.91 | 109637 | | 1108946 |
| 42 | | | 6.6 | 89.8 |
| 43 | | | 3.8 | 92.6 |
| 44 | | | 3.3 | 93.1 |
| 44+80± | Side Road | | 3.2 | 93.2 |
| 45 | | | 2.9 | 93.5 |
| | 8.18 | 110344 | 1.11 | 1095.26 |
| 46 | | | 8.3 | 95.1 |
| 46+02± | 60° S. Ditch to North across Rd. Culvert from pipe | | 8.2 | 95.2 |
| 47 | | | 5.8 | 97.6 |
| 48 | | | 3.8 | 99.6 |
| B.M. 7 | | | 4.15 | 1099.29 1099.32 |

30/6.5 11/7.6 10/8.4 6/7.6 —/6.6 7/7.3 10/8.7 12/7.3 17/6.4 30/6.0

30/4.0 12/4.1 10/5.3 —/3.8 6/4.8 8/5.9 11/3.5 20/1.7 30/1.6

30/4.7 12/3.7 10/4.2 —/3.3 7/4.1 9/3.4 30/2.3

200/4.4 150/4.3 100/3.8 50/3.5 —/3.2

30/3.5 20/2.6 13/4.1 10/3.3 —/2.9 6/3.5 12/2.4 25/1.4 30/1.4

30/8.5 14/8.2 11/9.6 8/8.7 —/8.3 7/8.7 8/8.3 30/7.1

Top of Pipe

30/6.9 4.1 Pvt 12" F.L. 7.0 9/7.5 —/9.2 —/8.3 —/8.2 —/8.2 T.P. 10/8.8 F.L. 10.0 13" 10.1 18" 8.3 50 Ft. W.I. D.T.H. 10.6

30/6.5 12/5.6 9/7.7 7/6.5 —/5.8 8/6.6 10/7.4 14/5.6 30/5.0

30/5.8 10/4.7 9/5.6 6/4.5 —/3.8 8/4.4 10/5.5 13/4.8 20/5.0 30/4.1

| | | | | |
|---|---|---|---|---|
| B.M.7 | 4.15 | 1103.47 | | 1099.32 |
| 49 | | | 3.0 | 00.5 |
| 50 | | | 1.8 | 01.7 |
| | 12.47 | 1114.93 | 1.01 | 1102.46 |
| 51 | | | 11.4 | 03.5 |
| 52 | | | 9.3 | 05.6 |
| 53 | | | 5.9 | 09.0 |
| | 12.31 | 1125.05 | 2.19 | 1112.74 |
| 54 | | | 12.6 | 12.5 |
| 55 | | | 9.8 | 15.3 |
| 56 | | | 7.2 | 17.9 |
| 57 | | | 3.4 | 21.7 |
| | 10.37 | 1135.21 | 0.21 | 1124.84 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 30/4.6 | 9/3.7 | 7.5/4.4 | 6/3.7 | — | 8/3.5 | 11/4.2 | 12/3.8 | 17/4.2 | 30/4.3 |
| 30/2.6 | 9/2.5 | 7/3.2 | 6/2.3 | —/1.8 | 9/2.2 | 11/3.1 | 12/2.4 | 30/3.1 | |
| 30/11.8 | 13/12.6 | 10/12.0 | 8/13.0 | 6/12.2 | —/11.4 | 7/12.2 | 11/13.1 | 12/12.2 | 30/11.9 |
| 30/9.0 | 11/9.4 | 9/11.0 | 6/9.9 | —/9.3 | 9/9.8 | 12/11.0 | 13/9.4 | 19/8.3 | 30/8.2 |
| 30/5.2 | 11/5.8 | 8/8.1 | 6/7.0 | —/5.9 | 9/6.3 | 11-13/7.2 | 14/4.7 | 20/3.9 | 30/3.1 |
| 30/11.9 | 9/12.4 | 7/15.1 | 5/13.2 | —/12.6 | 11/13.0 | 12/13.8 | 13/12.7 | 19/11.3 | 30/11.1 |
| 30/8.6 | 9/10.1 | 7/11.3 | 4/10.4 | —/9.8 | 9/10.2 | 12/11.2 | 14/9.2 | 20/8.8 | 30/88 |
| 30/5.6 | 12/6.0 | 7.5/8.3 | 4/7.7 | —/7.2 | 10/7.9 | 12/8.5 | 14/6.9 | 17/6.1 | 20/5.6 | 30/5.6 |
| 30/1.3 | 13/1.7 | 8.5/5.1 | 6/3.9 | —/3.4 | 9/4.1 | 12/4.9 | 17/1.3 | 30/1.0 | |

| | | | | | |
|---|---|---|---|---|---|
| | | 1135.21 | | | |
| 58 | | | 9.0 | 26.2 | |
| 59 | | | 5.5 | 29.7 | |
| B.M.# 8 | | | 9.80 | 1125.41 | 1125.43 |
| | 9.80 | 1135.23 | | | |
| 59+85 ± | | | 4.6 | 30.6 | |
| 60 | | | 4.2 | 31.0 | |
| | 10.01 | 1141.74 | 3.50 | 1131.73 | |
| 61 | | | 7.2 | 34.5 | |
| | 8.17 | 1146.64 | 3.27 | 1138.47 | |
| 62 | | | 8.3 | 38.3 | |
| 63 | | | 3.2 | 43.4 | |
| | 11.39 | 1157.60 | 0.43 | 1146.21 | |
| 64 | | | 10.2 | 47.4 | |
| 65 | | | 3.6 | 54.0 | |
| B.M. 9 | 2.99 | 1157.60 | 2.99 | 1154.61 | 1154.61 |

30 14 10 7 10 15 20 30
6.0 6.5 10.9 9.8 9.0 10.6 6.5 6.2 5.5

50 30 12 11 9 9 30 50
2.0 2.4 6.0 6.9 6.3 5.5 6.2 12.2 14.7

on R. Bank
30 25 15 11 FL 9 T.S. 7.5 FL 25 50
0.0 0.5 3.4 5.8 5.9 5.2 7.6 5.5 6.6 10.1 14.8
Inlet ditch West 1129.3 1128.7

30 27 22 14 11 9 6 8 22 30
0.1 0.3 2.6 3.4 5.6 4.9 4.2 4.8 4.6 7.3 9.2

30 15 13 8 8 30 50
4.2 7.0 7.8 7.3 7.2 8.1 10.8 13.9

30 23 15 10 7 9 13 18 30
1.5 3.2 7.2 10.1 8.3 9.3 9.8 8.1 7.9 8.8

+2.0 16 10 8 10 30
30 1.4 5.0 3.2 4.7 4.2 6.1

30 22 10 7 7 10 12 14 18 30
4.9 5.9 12.2 11.6 10.2 11.2 12.0 11.6 10.7 10.1 11.3

35 15 12 6 9 12 30
0.1 5.0 5.8 3.6 4.5 5.7 3.2 3.5

| | | | | | |
|---|---|---|---|---|---|
| | | 1157.60 | | | |
| | 9.77 | 1166.73 | 0.64 | 1156.96 | |
| 66 | | | 9.5 | 57.2 | |
| 67 | | | | | |
| | 1.56 | 1155.37 | 12.92 | 1153.81 | |
| 67 | | | 4.5 | 50.9 | |
| 67+60 ± | | | 5.5 | 49.9 | |
| 68 | | | 4.5 | 50.9 | |
| | 9.29 | 1164.62 | 0.04 | 1155.35 | |
| 69 | | | 6.9 | 57.7 | |
| | 11.44 | 1175.62 | 0.44 | 1164.18 | |
| 69 | | | | | |
| 70 | | | 9.4 | 66.2 | |
| B.M.10 | 1.12 | 1175.63 | 1.12 | 1174.50 | 1174.51 |
| | 12.65 | 1186.12 | 2.16 | 1173.47 | |
| 71 | | | 12.1 | 74.0 | |

30/2.9 25/3.3 14/9.7 12/10.8 11/10.3 9.5 8/11.4 12/7.7 30/12.7

35/4.3 20/10.6

14/5.0 12/4.5 6/3.7 0/4.5 2/4.6 20/14.9 30/17.5

T. of Headwall

50/12.3 F.L./15.4 T. of O./11.2 21/7.3 20/7.7 16/5.6 5.5 10/8.0

T. of Headwall

11/7.3 T. of O./12.1 F.L./15.3 50/16.5 100/17.7

1140.6 1140.1

30/11.4 24/10.9 11/4.9 3/4.2 4.5 3/5.2 17/6.6 38/12.4

50/11.3 40/6.3 36/6.3 29/7.4 6/6.3 6.9 2/7.5

22/6.7 30/5.8 50/4.3

30/1.8 24/1.8 13/10.2 4/8.9 9.7 3/10.3 4/8.3 16/0.60 30/0.02 40/0.00

30/14.9 14/11.6 12/13.8 9/13.2 12.1 7/13.7 14/9.7 30/8.2

| | | | | |
|---|---|---|---|---|
| | | 1186.12 | | |
| 72 | | | 5.2 | 80.9 |
| | 13.03 | 1195.51 | 3.64 | 1182.48 |
| T. P. | | | 5.63 | 1189.88 |

$\frac{30}{6.1}$ $\frac{15}{4.5}$ $\frac{11}{7.3}$ $\frac{7}{5.9}$ $\frac{}{5.2}$ $\frac{8}{7.0}$ $\frac{15}{1.9}$ $\frac{30}{0.7}$

R.P. Hub 30' Lt. Sta. 73+20

Nov. 15, 1930
D. Parks
R. Hassel
T. Snyder



| | | | | | |
|---|---|---|---|---|---|
| T.P. | 6.14 | 1196.02 | | 1189.88 | |
| 73 | | | 8.8 | 87.2 | |
| | 0.20 | 1187.07 | 9.15 | 1186.87 | |
| 74 | | | 6.6 | 80.5 | |
| 74+92 | Culvert | | 10.7 | 76.4 | |
| 75 | | | 10.8 | 76.3 | |
| | 7.56 | 1183.99 | 10.64 | 1176.43 | |
| 76 | | | 7.9 | 76.1 | |
| B.M. #11 | 6.19 | 1183.97 | 6.19 | 1177.80 | 1177.78 |
| 76+76± | Cross road | | 5.1 | 78.9 | |
| 77 | | | 4.2 | 79.8 | |
| | 11.47 | 1192.55 | 2.89 | 1181.08 | |
| 78 | | | 8.8 | 83.8 | |
| 79 | | | 5.1 | 87.5 | |

30 / 6.5 — 14 / 6.2 — 10 / 9.9 — 8.8 — 8 / 9.4 — 16 / 4.7 — 30 / 3.9

30 / 7.4 — 13 / 5.6 — 14 / 8.5 — 5 / 6.9 — 6.6 — 10 / 7.9 — 16 / 2.6 — 30 / 1.5

100 / 15.8 — 50 / 15.1 — 20 / 13.8 — F.L. / 13.3 — T.P. 8 / 12.3 — 10.7 — 8 / 10.6 — T.P. 15 / 12.1 — F.L. / 12.8 — B 15 / 11.8 — 30 / 12.3

1173.8 — 1174.3 — inlet from ditch

30 / 11.6 — 15 / 12.2 — 12-8 / 13.4 — 6 / 11.8 — 10.8 — 8 / 10.6 — 15 / 12.7 — 17 / 12.0 — 30 / 12.2

30 / 8.0 — 16 / 8.9 — 13-9 / 9.7 — 7 / 7.6 — 7.9 — 6 / 7.5 — 18 / 9.0 — 20 / 8.2 — 30 / 8.7

200 / 3.7 — 150 / 2.3 — 100 / 3.3 — 50 / 4.4 — 5.1 — 50 / 3.9 — 100 / 2.7 — 150 / 1.4 — 175 / 1.3 — 200 / 1.8 — 250 / 4.2

30 / 3.0 — 14 / 3.7 — 8 / 4.9 — 4.2 — 14 / 5.2 — 20 / 3.6 — 30 / 2.3

30 / 6.9 — 16 / 6.7 — 12 / 10.2 — 10 / 8.6 — 8.8 — 7 / 9.4 — 8 / 10.1 — 16 / 6.0 — 30 / 5.1

30 / 5.2 — 16 / 4.3 — 13 / 6.1 — 11 / 5.6 — 3 / 4.6 — 5.1 — 4 / 5.5 — 7 / 6.2 — 10 / 4.4 — 13 / 3.9 — 30 / 2.9

| | | | | | |
|---|---|---|---|---|---|
| | | 1192.55 | | | |
| 80 | | | 2.8 | 89.8 | |
| | 9.35 | 1202.85 | 1.05 | 1191.50 | |
| 81 | | | 9.4 | 91.5 | |
| 82 | | | 6.9 | 94.0 | |
| 83 | | | 4.8 | 96.1 | |
| | 3.79 | 1198.99 | 5.65 | 1195.20 | |
| B.M. #12 | 4.77 | 1199.01 | 4.77 | 1194.22 | 1194.24 |
| 84 | | | 6.2 | 92.8 | |
| 85 | | | 7.2 | 91.8 | |
| 85+63 | | | 5.7 | 93.3 | |
| 86 | | | 5.0 | 94.0 | |
| | 12.93 | 1210.67 | 1.27 | 1197.74 | |
| 87 | | | 13.0 | 97.7 | |

30/3.6 16/2.7 13/3.6 12/3.0 5/2.3 2/2.8 — 3/3.1 5/3.8 8/1.9 30/1.3

30/8.8 17/8.7 15/10.1 6/8.8 9/9.4 — 5/10.2 18/8.5 30/8.5

30/6.0 17/6.0 13/7.8 4/6.5 6/6.9 — 6/7.9 9/5.9 19/5.2 28/6.1 30/5.9

30/3.9 18/4.1 14/4.8 4/4.4 4/4.8 — 5/5.1 7/3.5 30/4.2

30/1.6 19/2.3 12/6.9 6/6.2 — 7/7.2 15/3.8 30/7.6

30/6.7 18/7.5 15/7.8 12/7.3 4/6.8 7/7.2 — 5/7.5 21/9.5 30/9.7

Ft. of T.I. to inlet ditch; T. of H.W.; T. of H.W.

65/9.0 60/9.6 Ft./9.1 T. of H./6.9 13/4.8 11/5.9 5/5.7 — 6/5.7 75/4.6 T. of H./6.9 Ft./8.7 30/9.2 50/9.6 100/11.1

1189.9 1190.3

30/6.4 14/6.0 10/5.1 5/5.0 — 7/5.7 27/5.5 40/1.7

30/13.8 20/12.4 14/12.5 10/13.5 13/13.0 — 6/14.5 9/13.7 14/10.7 30/8.8

| | | | | | |
|---|---|---|---|---|---|
| | | 1210.67 | | | |
| 88 | | | 8.1 | 02.6 | |
| | 12.12 | 1218.29 | 4.50 | 1206.17 | |
| 89 | | | 11.8 | 06.5 | |
| 90 | | | 7.2 | 11.1 | |
| 91 | | | 7.9 | 10.4 | |
| B.M #13 | 6.02 | 1215.52 | 8.86 | 1209.43 | 1209.50 |
| 91+47± | | | 4.9 | 10.6 | |
| 92 | | | 4.6 | 10.9 | |
| 93 | | | 3.5 | 12.0 | |
| | 11.11 | 1225.72 | 0.91 | 1214.61 | |
| 94 | | | 9.4 | 16.3 | |
| 95 | | | 5.4 | 20.3 | |
| 96 | | | 3.7 | 22.0 | |

30/10.1 21/8.4 12/7.6 8/9.1 —/8.1 7/8.6 8-10/9.1 16/5.5 30/4.2

30/14.3 9/11.3 6/12.3 —/11.8 9/12.1 12/12.8 17/9.2 26/7.0 30/7.4

30/15.1 19/7.1 7/8.4 —/7.2 11/8.3 17/4.2 30/2.5

30/11.0 10/9.8 8/8.8 —/7.9 8/8.4 14/8.3 24/3.2 30/2.7

150. 12.8 7.5 / 12.8 12.8 9.9 — in D.T.H. 30/7.1 F.L./9.0 T.O./6.5 — T. of H.W. 12/4.3 10.5/5.1 —/4.9 8/4.9 9/4.1 T.O./6.2 F.L./8.9 30/7.3 50/7.1 — T. of H.W. 1206.5 — 1206.6

30/6.8 12/5.7 11/6.2 9/5.5 —/4.6 10/5.5 11/4.9 19/6.0 30/6.4

30/0.4 13/2.4 9/4.8 7/3.7 —/3.5 18/4.2 20/3.6 30/5.1

30/4.7 21/5.1 12/11.0 9/9.8 —/9.4 6/9.6 11/11.5 18/7.0 30/7.7

30/4.2 13/6.2 11/7.1 7/5.7 —/5.4 6/6.1 8/7.2 11/5.8 30/6.2

30/2.6 12/4.0 10/5.6 7/4.2 —/3.7 8/5.0 11/4.1 30/5.1

| | | | | | |
|---|---|---|---|---|---|
| | | 1225.72 | | | |
| | 8.24 | 1232.13 | 1.83 | 1223.89 | |
| 97 | | | 8.0 | 24.1 | |
| 98 | | | 5.5 | 26.6 | |
| 99 | | | 4.5 | 27.6 | |
| 99+21± | culvert | | 4.2 | 27.9 | |
| 100 | | | 3.4 | 28.7 | |
| | 5.45 | 1234.34 | 3.24 | 1228.89 | |
| B.M. #14 | 1.94 | 1234.39 | 1.94 | 1232.40 | 1232.45 |
| 101 | | | 4.9 | 29.5 | |
| 102 | | | 3.2 | 31.2 | |
| 103 | | | 1.5 | 32.9 | |
| | 13.07 | 1246.71 | 0.75 | 1233.64 | |
| 104 | | | 11.6 | 35.1 | |

| | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 30 / 4.9 | 13 / 8.0 | 11 / 9.4 | 9 / 8.7 | 8.0 | 7 / 8.6 | 9 / 9.7 | 13 / 7.7 | 30 / 8.8 | | | |
| 30 / 3.7 | 13 / 5.3 | 9 / 7.6 | 7 / 6.3 | 5.5 | 8 / 6.2 | 10 / 7.6 | 13 / 6.3 | 30 / 6.9 | | | |
| 30 / 4.3 | 12 / 5.3 | 10 / 6.1 | 7 / 4.8 | 4.5 | 6 / 4.8 | 9 / 5.9 | 11 / 5.0 | 30 / 6.3 | | | |
| Side Bank 50 / 3.3 | Ditch 15 / 4.9 | 50 / 5.4 | FL. 6.0 | 10.7 Natural 4.9 | 4.2 | 8 / 5.0 | FL. 6.3 | 20 / 6.8 | 50 / 7.7 | 100 / 8.5 | 200 / 10.4 |
| | | | 1226.1 | | | | 1225.8 | | | | |
| 30 / 3.6 | 12 / 4.0 | 10 / 4.7 | 7 / 4.0 | 3.4 | 5 / 3.5 | 8 / 4.9 | 10 / 3.9 | 20 / 4.6 | 30 / 3.8 | | |
| 30 / 4.5 | 12 / 5.0 | 10 / 5.9 | 8 / 5.4 | 4.9 | 7 / 6.3 | 8 / 6.0 | 12 / 5.6 | 17 / 5.4 | 30 / 3.9 | | |
| 30 / 2.9 | 12 / 3.4 | 10 / 4.7 | 3.2 | 7 / 3.6 | 10 / 4.4 | 16 / 2.7 | 30 / 2.0 | | | | |
| 30 / 0.00 | 15 / 0.11 | 9 / 2.8 | 1.5 | | 11 / 2.5 | 15 / 1.6 | 30 / 1.3 | | | | |
| 30 / 10.4 | 15 / 10.4 | 10 / 13.1 | 8 / 12.5 | 11.6 | | 12 / 13.1 | 16 / 11.3 | 30 / 11.2 | | | |

| | | | |
|---|---|---|---|
| | 124671 | | |
| 105 | | 95 | 37.2 |
| 106 | | 6.5 | 402 |
| 107 | | 3.1 | 436 |
| 108 | | 2,3 | 444 |
| T. P. | | 3,10 | 124361 |

30/8,3 16/8,3 12/11.1 9/10.3 9,5

10/10.7 15/8,5 30/8,5

30/5,5 15/5,3 11/8,3 8/7.5 6,5

11/7,9 15/5,2 30/5,1

38/2,9 14/2,7 10/4,6 3,1

11/4,8 15/2,4 30/2,0

30/2,7 13/2,3 10/3,3 2,3

11/3,7 14/2,4 30/2,0

R. P. Hub ℄ sta 108+65± 30' Lt of ℄

| | | | | |
|---|---|---|---|---|
| T.P | 2.27 | 124588 | | 1243.61 |
| 109 | | | 4.1 | 418 |
| 110 | | | 8.6 | 373 |
| 111 | | | 10.9 | 35.0 |
| | 1.17 | 1234.75 | 12.30 | 1233.58 |
| 112 | | | 1.8 | 33.0 |
| 113 | | | 4.0 | 30.8 |
| 114 | | | 5.5 | 29.3 |
| 115 | | | 6.7 | 28.1 |
| 116 | | | 8.0 | 26.8 |
| | 4.04 | 1230.55 | 8.24 | 1226.51 |
| 117 | | | 4.8 | 25.8 |

Nov. 18 1930
D. Parks
R. Hasse)
T. Snyder



R.P. Hub Lt. sta. 108+65 ± 30' Lt.

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| 30 | 16 | 13 | 8 | | | | 10 | 13 | 30 | |
| 3.1 | 3.1 | 2.5 | 5.6 | 4.1 | | | 5.2 | 2.9 | 2.9 | |
| | 30 | 10 | 7 | | | | 9 | 14 | 30 | |
| | 7.2 | 8.1 | 9.3 | 8.6 | | | 9.7 | 7.4 | 7.2 | |
| 30 | 9 | 8 | 6 | | | 9 | 14 | 30 | | |
| 11.8 | 11.3 | 12.0 | 11.5 | 10.9 | | 12.2 | 10.0 | 9.6 | | |
| | 30 | 9 | 7 | | | 7 | 12 | 30 | | |
| | 2.0 | 1.9 | 2.8 | 1.8 | | 3.1 | 1.1 | 0.4 | | |
| 30 | 8 | 6 | 5 | | | 8.5 | 14 | 30 | | |
| 4.5 | 3.8 | 4.9 | 7.5 | 4.0 | | 4.2 | 2.4 | 1.7 | | |
| | 30 | 9 | 7 | | | 10 | 14 | 30 | | |
| | 6.2 | 5.7 | 6.4 | 5.5 | | 6.3 | 4.2 | 3.4 | | |
| 30 | 10 | 7 | 4 | | 8 | 11 | 12 | 30 | | |
| 7.4 | 7.2 | 7.9 | 6.9 | 6.7 | 7.1 | 7.7 | 6.9 | 6.2 | | |
| 30 | 9.5 | 8 | 6 | | 9 | 11 | 12.5 | 30 | | |
| 7.2 | 7.7 | 9.2 | 8.7 | 8.0 | 8.6 | 8.9 | 8.2 | 8.8 | | |
| 30 | 13 | 6 | 4 | | 2 | 11 | 12.5 | 30 | | |
| 2.7 | 3.1 | 6.1 | 5.3 | 4.8 | 4.4 | 5.5 | 4.6 | 4.7 | | |

| | | | | | |
|---|---|---|---|---|---|
| | | 1230.55 | | | |
| 118 | | | 9.1 | 21.5 | |
| B.M. #15 | 6.78 | 1230.55 | 6.78 | 1223.77 | 1223.77 |
| 119 | | | 14.6 | 16.0 | |
| | 1.24 | 1218.82 | 12.97 | 1217.58 | |
| 120 | | | 6.0 | 12.8 | |
| 121 | | | 8.7 | 10.1 | |
| 122 | | | 11.0 | 07.8 | |
| | 3.69 | 1209.69 | 12.82 | 1206.00 | |
| 123 | | | 4.7 | 05.0 | |
| 124 | | | 7.4 | 202.3 | |
| 125 | | | 11.0 | 1198.7 | |
| | 1.14 | 1198.56 | 12.27 | 1197.42 | |
| 126 | | | 4.8 | 93.8 | |
| 127 | | | 9.7 | 88.9 | |

$\frac{30}{5.7}$ $\frac{20}{4.8}$ $\frac{12}{10.0}$ $\frac{9}{9.6}$ $\frac{}{9.1}$ $\frac{5}{9.1}$ $\frac{6}{8.4}$ $\frac{10}{8.5}$ $\frac{13}{9.7}$ $\frac{18}{5.7}$ $\frac{30}{5.2}$

$\frac{30}{11.4}$ $\frac{23}{11.0}$ $\frac{15}{14.5}$ $\frac{10}{15.6}$ $\frac{8}{14.9}$ $\frac{}{14.6}$ $\frac{7}{14.8}$ $\frac{10}{15.4}$ $\frac{15}{12.3}$ $\frac{30}{12.0}$

$\frac{30}{5.9}$ $\frac{17}{5.2}$ $\frac{13}{6.0}$ $\frac{10}{7.8}$ $\frac{8.5}{6.8}$ $\frac{}{6.0}$ $\frac{4}{6.5}$ $\frac{6.5}{7.2}$ $\frac{10}{5.5}$ $\frac{30}{5.6}$

$\frac{30}{9.0}$ $\frac{16}{8.0}$ $\frac{12}{8.9}$ $\frac{10}{10.5}$ $\frac{8}{9.6}$ $\frac{}{8.7}$ $\frac{6}{9.1}$ $\frac{7}{10.2}$ $\frac{10}{7.8}$ $\frac{30}{7.7}$

$\frac{30}{10.3}$ $\frac{18}{9.6}$ $\frac{13}{11.1}$ $\frac{11}{12.9}$ $\frac{8}{12.1}$ $\frac{}{11.0}$ $\frac{4}{11.5}$ $\frac{7}{12.6}$ $\frac{13}{9.4}$ $\frac{30}{8.4}$

$\frac{30}{3.4}$ $\frac{19}{2.3}$ $\frac{11}{6.6}$ $\frac{9}{5.2}$ $\frac{}{4.7}$ $\frac{4}{4.9}$ $\frac{7}{6.3}$ $\frac{12.5}{3.3}$ $\frac{30}{2.6}$

$\frac{30}{5.0}$ $\frac{21}{4.6}$ $\frac{13}{9.0}$ $\frac{5}{7.2}$ $\frac{}{7.4}$ $\frac{4}{7.7}$ $\frac{7}{9.0}$ $\frac{13}{6.0}$ $\frac{30}{5.3}$

$\frac{30}{7.2}$ $\frac{21}{6.9}$ $\frac{14}{12.1}$ $\frac{10}{11.3}$ $\frac{}{11.0}$ $\frac{3}{11.3}$ $\frac{6}{12.2}$ $\frac{12}{8.5}$ $\frac{30}{8.0}$

$\frac{30}{0.6}$ $\frac{20}{1.1}$ $\frac{12}{4.3}$ $\frac{9.5}{5.0}$ $\frac{}{4.8}$ $\frac{3}{5.1}$ $\frac{4}{6.2}$ $\frac{7}{4.6}$ $\frac{13.5}{2.1}$ $\frac{30}{2.3}$

$\frac{38}{4.7}$ $\frac{20}{4.9}$ $\frac{16}{8.6}$ $\frac{12.5}{11.2}$ $\frac{10}{10.0}$ $\frac{5}{9.2}$ $\frac{}{9.7}$ $\frac{4}{10.3}$ $\frac{4.5}{11.0}$ $\frac{11}{7.2}$ $\frac{30}{7.5}$

| | | | | | |
|---|---|---|---|---|---|
| | | 1198.56 | | | |
| 128 | | | 14.0 | 84.6 | |
| | 1.58 | 1187.40 | 12.74 | 1185.82 | |
| 129 | | | 4.9 | 82.5 | |
| 130 | | | 6.6 | 80.8 | |
| 130+68 | | | 7.5 | 79.9 | |
| 131 | | | 8.0 | 72.4 | |
| 132 | | | 8.0 | 79.4 | |
| | 4.60 | 1179.74 | 12.26 | 1175.14 | |
| 133 | | | 3.1 | 76.6 | |
| 134 | | | 5.1 | 74.6 | |
| B.M. #16 | 5.39 | 1179.76 | 5.39 | 1174.35 | 1174.37 |
| 134+55 | | | 5.2 | 74.6 | |
| | 4.85 | 1180.16 | 4.45 | 1175.31 | |

30/10.5 23/10.3 17/12.3 13/15.1 11/14.7 5/13.6 14.0 3/14.1 5.5/14.5 10/12.6 30/17.0

30/3.8 19/5.0 17/6.2 13/6.1 7/4.5 4.9 3.5/5.7 6/5.2 30/6.1

30/7.8 18/7.0 16/8.3 14/7.4 6.6 7/6.8 30/7.9

300/13.5 200/11.5 100/10.9 50/11.1 F.L./10.2 T.O./9.6 7 H.W./6.9 16/7.4 7.5 4/7.4 H.W./6.7 T.O./9.3 F.L./10.2 50/8.1 100/8.0

1177.2 1077.2

30/9.0 22/7.9 15/8.6 13/7.9 5/7.6 8.0 2/7.9 4/8.4 8/8.6 13.5/7.2 30/6.9

30/9.2 12/8.6 9/9.3 7/8.5 8.0 8/8.3 12/9.7 15/8.2 30/7.4

30/3.3 10/2.8 6.5/7.1 4/3.2 3.1 11.5/3.7 14/4.7 16/3.1 20/2.0 30/0.5

30/6.7 13/6.7 10/7.0 8/6.1 5.1 8/5.7 10/6.2 13/6.0 30/5.5

100/10.2 50/8.3 F.L./7.5 T.O.S.R./4.8 7.0/6.2 5.2 80/6.0 H.W./6.4 F.L./7.3 15/6.9 30/6.3 STORM WATER INFLOW 30/6.7

1172.3 1172.5

| | | | | |
|---|---|---|---|---|
| | | 1180.16 | | |
| 135 | | | 5.5 | 74.7 |
| 136 | | | 5.7 | 745 |
| 137 | | | 4.6 | 75.6 |
| 138 | | | 4.3 | 75.9 |
| 139 | | | 4.1 | 76.1 |
| 140 | | | 3.6 | 76.6 |
| | 5.91 | 1184.07 | 2.00 | 1178.16 |
| 141 | | | 6.2 | 77.9 |
| 142 | | | 4.5 | 79.6 |
| 143 | | | 8.6 | 75.5 |
| 144 | | | 13.3 | 70.8 |

30/7.6 13/7.1 12/7.6 10/6.6 —/5.5 6/6.2 9/6.8 12/7.0 13/6.4 30/6.1

30/7.1 13/6.7 11/7.5 9/6.7 —/5.7 8/6.9 13/6.3 30/5.7

30/5.2 12/5.1 10/6.6 8/5.8 —/4.6 11/6.0 13/5.3 30/4.6

30/5.2 13/4.9 10/5.9 7/4.9 —/4.3 13/5.4 15/4.9 30/4.6

30/5.5 12/5.0 10/5.6 7/4.9 —/4.1 9/4.8 13/5.1 15/4.7 30/4.2

30/3.8 12/3.8 9.5/5.0 —/3.6 12/4.7 16/3.6 30/2.8

30/5.3 11/6.1 9/7.1 —/6.2 12/7.0 15/5.4 30/4.3

30/4.4 16/4.2 10/4.6 8/6.0 —/4.5 12/5.7 16.5/4.1 30/3.5

30/6.6 12/7.3 9/9.1 6/9.6 5/9.2 —/8.6 8/9.0 13.5/9.8 17/7.4 30/7.1

30/9.2 16/10.5 10-8/15.0 5/13.9 —/13.3 11/14.9 15/11.9 30/11.5

| | | | | | |
|---|---|---|---|---|---|
| | | 1184.07 | | | |
| | 2.15 | 1173.58 | 12.64 | 1171.43 | |
| 145 | | | 5.8 | 67.8 | |
| 145+12 | Culvert | | 6.0 | 676 | |
| 145+28.31 | | | 6.5 | 67.1 | |
| B.M #17 | 4.71 | 1173.63 | 4.71 | 1168.87 | 1168.92 |
| T.P | 5.37 | 1179.00 | 0.00 | 1173.63 | |
| B.M #17 | | | 4.28 | 1174.72 | 1174.73 |
| B.M #17 | 0.10 | 1169.02 | | 1168.92 | |
| 146 | | | 5.1 | 63.9 | |
| 147 | | | 7.8 | 61.2 | |
| 148 | | | 10.1 | 58.9 | |
| | 3.68 | 1159.75 | 12.95 | 1156.07 | |
| 149 | | | 4.0 | 55.8 | |
| 150 | | | 8.4 | 51.4 | |

30/3.9 13/6.6 8/6.3 5.8 12.5/7.4 18/7.1 30/6.4

50/6.1 25/7.2 F.L./8.5 T.P./7.7 12.5/6.9 6.0 11/7.2 14/7.5 T.P. 15/8.0 F.L./8.7 25/9.4 50/10.6

1165.1 75/11.3 100/12.3

200/0.0 175/0.5 150/1.1 100/2.5 50/4.7 1167.08/6.5 100/10.1 200/13.1

30/2.0 26/2.5 23/4.6 15.5/5.8 14/5.2 (1164.92) 5.1 7/5.6 10/4.6 30/4.7

30/5.7 24/6.1 16/7.8 14/8.8 13/7.9 (1162.22) 7.8 7.5/8.5 9/7.9 30/9.4

30/7.8 15/10.1 13/10.9 11/10.4 (1159.92) 10.1 5/10.7 7/10.3 21/10.5 30/11.6

30/0.2 28/0.4 15.5/4.2 13/5.3 12/4.5 (1155.75) 4.0 6/4.7 8.5/3.6 15/3.5 30/5.0

30/4.7 15/8.8 13/8.6 6/7.9 (1151.35) 8.4 4/8.7 7/8.0 30/10.3

| | | | | |
|---|---|---|---|---|
| | 1159.75 | | | |
| B.M #19 | | 8.34 | 1151.41 | 1151.45 |

| | | | | |
|---|---|---|---|---|
| B.M. #19 | 3.07 | 1154.52 | | 1151.45 |
| 151 | | | 6.9 | 47.7 |
| 152 | | | 10.4 | 44.2 |
| | 3.66 | 1145.42 | 12.69 | 1141.83 |
| 153 | | | 9.9 | 35.6 |
| 154 | | | | |
| 155 | | | | |
| | 1.58 | 1134.53 | 12.54 | 1132.95 |
| 154 | | | 4.0 | 30.6 |
| 155 | | | 4.0 | 30.6 |
| 156 | | | 7.4 | 26.7 |
| | 3.48 | 1130.10 | 7.91 | 1126.62 |
| 156+70 | | | 3.9 | 26.2 |

Nov. 19, 1930
D. Parks
T. Snyder
F. Gray

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(1147.62)

30/2.7 27/4.3 17/7.1 14/6.3 7/6.0 /6.9 4/7.2 7/6.5 1/30/10.6

30/7.2 20/9.5 13/9.9 12/10.7 5/10.2 (1144.12) /10.4 6/10.8 10/8.2 30/11.7

40/0.8 30/1.8 15/9.7 11.5/9.7 7/11.0 7/10.2 1135.60/9.9 7/10.3 8/8.4 14/4.5 30/4.7

40/4.9 30/7.1 22/9.2

see additional levels at back of book

35/+4.3 26/2.8 16/5.6

1130.53
14/3.3 5/5.6 3/5.0 2/4.2 /4.0 6/3.6 14/4.2 15/3.9 30/4.8

1130.53
/4.0 5/6.9 13/5.8 30/6.6

(1126.63)
35/+6.5 25/0.9 15/8.3 10/9.0 8/8.2 /7.9 4/7.4 10/7.9 21/9.0 25/12.1 34/12.2 40/10.8

(1126.20)
150/8.5 100/8.4 50/8.6 20/8.6 F.L./8.6 Tot 0/4.9 9.5/3.4 7.5/3.4 /3.9 7/3.8 9.5/3.2 Tot 0, F.L./4.8 25/8.5 30/8.1 Front 50/6.3 7.9/10.0 9.7

1121.5 1125.2 1125.3

| | | | | | |
|---|---|---|---|---|---|
| | | 1130.10 | | | |
| 157 | | | 4.7 | 25.4 | |
| 158 | | | 4.3 | 25.8 | |
| | 10.24 | 1138.04 | 2.30 | 1127.80 | |
| B.M. #20 | 10.51 | 1138.04 | 10.51 | 1127.53 | 1127.53 |
| 159 | | | 10.6 | 27.4 | |
| | 8.27 | 1145.99 | 0.32 | 1137.72 | |
| 160 | | | 12.5 | 33.5 | |
| 161 | | | 7.9 | 38.1 | |
| 162 | | | 2.9 | 43.1 | |
| | 9.76 | 1154.70 | 1.05 | 1144.24 | |
| 163 | | | 7.2 | 47.5 | |
| 1637.50 | | | 4.9 | 49.8 | |
| 164 | | | 4.6 | 50.1 | |
| | 4.32 | 1154.09 | 5.03 | 1149.67 | |



(1125.40)

30/6.2 9/5.5 7/4.9 —/4.7 10/5.1 12.5/5.7 26/6.2 30/5.5

(1125.80)

30/6.2 17/5.7 14/4.8 —/4.3 30/5.4

(1127.44)

30/11.6 15/10.8 5/10.2 —/10.6 12/10.1 23/3.6 30/1.1 40/+2.1

(1133.49)

30/13.8 15/10.8 9/11.0 5/13.6 —/12.5 10/12.6 14/13.2 17/9.4 21/7.5 30/4.9

(1138.09)

30/7.6 24/6.9 5/7.1 —/7.9 5/5.8 30/2.8

1143.09

30/4.4 28/3.9 26/3.4 19/3.2 16/3.7 12/3.2 —/2.9 4.5/2.6 8/3.0 11/2.1 30/0.5

(1137.50)

30/5.2 23/5.3 17/7.8 14/6.9 —/7.2 5.5/7.8 11/3.9 30/3.0

(1149.80)

30/5.7 27/5.2 18/5.2 14.5/5.8 13/5.1 3.5/4.5 —/4.9 7.5/5.7 10.5/3.2 18/2.1 30/2.0

(1150.10)

30/6.2 23/5.4 17/5.6 10/5.2 —/4.6 11/5.5 16/3.5 30/2.9

| | | | | | |
|---|---|---|---|---|---|
| | | 1154.09 | | | |
| 165 | | | | | |
| 166 | | | | | |
| 167 | | Void | | | |
| 168 | | | | | |
| | 3.04 | 1144.30 | 12.83 | 1141.26 | |
| B.M. = 20 | | 1144.31 | 0.46 | 1143.84 | 1143.85 |
| 169 | | | | | |
| 170 | | | | | |
| | 2.12 | 1137.60 | 8.83 | 1135.48 | |
| 171 | | | | | |

$\frac{30}{5.6}$ $\frac{25}{5.3}$ $\frac{15}{5.8}$ $\frac{14}{5.4}$ $\frac{}{4.2}$ $\frac{12}{5.3}$ $\frac{18}{3.7}$ $\frac{30}{2.5}$

$\frac{30}{3.4}$ $\frac{18}{3.5}$ $\frac{10}{4.2}$ $\frac{4}{7.0}$ $\frac{}{6.4}$ $\frac{5}{5.9}$ $\frac{13}{6.3}$ $\frac{14}{7.4}$ $\frac{27}{3.3}$ $\frac{30}{3.0}$

$\frac{30}{7.9}$ $\frac{18}{7.7}$ $\frac{9}{8.2}$ $\frac{4}{10.5}$ $\frac{}{10.2}$ $\frac{5}{9.5}$ $\frac{15}{10.1}$ $\frac{16.5}{11.6}$ $\frac{18}{9.8}$ $\frac{30}{9.4}$

Void

$\frac{30}{9.8}$ $\frac{15}{9.8}$ $\frac{11}{10.1}$ $\frac{6}{11.1}$ $\frac{3}{13.3}$ $\frac{}{12.6}$ $\frac{4}{12.1}$ $\frac{11}{12.9}$ $\frac{14}{14.3}$ $\frac{18}{11.3}$ $\frac{30}{10.6}$

$\frac{30}{3.9}$ $\frac{10}{4.2}$ $\frac{5}{6.5}$ $\frac{3}{7.1}$ $\frac{}{6.9}$ $\frac{5}{6.4}$ $\frac{13}{6.9}$ $\frac{18}{6.7}$ $\frac{28}{4.5}$ $\frac{30}{3.7}$

$\frac{30}{9.3}$ $\frac{16}{9.1}$ $\frac{}{8.7}$ $\frac{18}{8.2}$ $\frac{30}{8.7}$

$\frac{18}{3.4}$ $\frac{19}{3.0}$ $\frac{30}{2.0}$

| | | | | | |
|---|---|---|---|---|---|
| | 3.93 | 1153.60 | | 1149.67 | |
| 165 | | | 3.8 | 49.8 | |
| 166 | | | 5.4 | 48.2 | |
| 167 | | | 3.1 | 44.5 | |
| 168 | | | 11.9 | 41.7 | |
| | 3.05 | 1144.22 | 12.43 | 1141.17 | |
| B.M. #21 | 047 | 114423 | 0.47 | 1143.75 | 1143.76 |
| 169 | | | 6.5 | 37.7 | |
| 170 | | | 7.9 | 36.3 | |
| 171 | | | 8.7 | 35.5 | |
| | 2.73 | 1136.73 | 10.23 | 1134.00 | |
| 172 | | | 2.6 | 34.1 | |
| 173 | | | 4.0 | 32.7 | |

(1149.80)

30/5.2 25/4.8 16/4.8 13.5/5.0 —/3.8 12/4.9 18/3.3 30/2.1

(1148.20)

30/3.8 25/3.0 17/3.8 12/6.6 —/5.9 7/5.9 10-11/7.0 13/5.1 22/2.6 30/2.9

(1144.50)

30/7.6 25/7.2 17/7.7 12/10.1 —/9.1 8.5/10.2 11/8.3 22/9.0 30/9.4

(1141.70)

30/9.6 22/9.7 15/10.4 14/13.0 9.5/12.3 —/11.9 3.5/12.5 6/13.9 9/11.0 22/10.2 30/10.7

(1138.73)

30/4.0 19/4.3 10.5/7.1 —/6.5 9.5/6.8 14/4.4 23/3.3 30/3.9

(1136.39)

30/9.2 10.5/8.7 —/7.9 10/8.2 20/8.7 30/8.9

(1136.50)

30/9.7 7/9.8 —/8.7 7/9.2 9.5/10.1 17/8.9 30/8.9

(1134.13)

30/1.9 19/2.3 12/4.3 10.5/3.9 —/2.6 9.5/3.9 13/2.4 22/2.1 30/2.4

1132.73

30/3.0 24/3.4 12/5.2 —/4.0 7/4.6 9/5.5 11/15.3 30/5.3

| | | | | | |
|---|---|---|---|---|---|
| | | 1136.73 | | | |
| 174 | | | 5.1 | 31.6 | |
| 175 | | | 7.9 | 28.8 | |
| 176 | | | 10.4 | 26.3 | |
| | 3.99 | 1130.22 | 10.50 | 1126.23 | |
| 177 | | | 4.5 | 25.7 | |
| B.M.#22 | | | 4.70 | 1125.52 | 1125.55 record |

(1131.63)

30/7.2 25/7.2 11/6.5 —/5.1 8/5.6 10-11/6.4 14/5.8 30/5.9

(1128.83)

30/7.5 17/7.5 13/8.8 10/7.8 —/7.9 11.5/8.4 17/6.6 30/6.9

(1126.33)

30/11.1 18/11.1 10/11.2 —/10.7 30/11.0

(1125.70)

30/6.7 17/6.1 10/5.6 9.5/5.9 8/5.1 —/4.5 10/5.0 12/5.6 14/5.1 16/5.6 30/6.3

| | BS | HI | FS | Richey Group Elev. | Corrected Elev. | |
|---|---|---|---|---|---|---|
| | Check levels | | | | | |
| BM 1 | 3.03 | 107.488 | | 107.185 | 1072.36 | Spike in root 18" Maple 30' Lt ℄ Sta 0+90 |
| | 5.65 | 107.140 | 9.13 | 106.575 | | |
| Sta 7 | | | 4.0 | 106.74 | | |
| BM 2 | 1.45 | 106.728 | 5.57 | 106.583 | 1066.34 | Spike in root 24" Maple 60' Lt ℄ Sta 9+60 |
| | 5.22 | 106.884 | 3.66 | 106.362 | | |
| 57+7 | | | 3.8 | 106.50 | | |
| | 7.76 | 107.334 | 3.26 | 106.558 | | |
| BM 3 | | | 7.10 | 106.634 | 1066.75 | SeW side 10" Hickory 30' Lt ℄ Sta 28+80 |
| Sta 24 | | | 4.2 | 106.93 | | |
| | 5.54 | 107.672 | 2.16 | 107.118 | | |
| BM 4 | | | 3.02 | 107.370 | 1074.21 | Spike in root 24" Maple 30' Rt ℄ Sta 26+30 |
| | 3.46 | 107.787 | 2.31 | 107.441 | | |
| BM 5 | | | 3.27 | 107.460 | 1075.11 | Spike in root 24" Maple 27' Rt ℄ Sta 32+90 |
| | 7.00 | 1080.97 | 3.90 | 107.397 | | |
| | 10.82 | 108.047 | 1.32 | 107.365 | | |
| BM 6 | 8.05 | 108.780 | 1.52 | 108.895 | 1083.46 | Spike in root 24" Maple 30' Lt ℄ Sta 41+50 |
| | 8.89 | 110.365 | 2.29 | 108.476 | | |
| BM 7 | | | 4.84 | 108.881 | 1092.32 | Spike in root 18" Maple 25' Lt ℄ Sta 48+15 |
| | 10.26 | 111.186 | 2.05 | 110.160 | | |

| | | | | | Corrected Elev. | |
|---|---|---|---|---|---|---|
| | | 1111.86 | | | | |
| | 10.22 | 1121.82 | 0.26 | 1111.60 | | |
| | 11.62 | 1133.39 | 0.05 | 1121.77 | | |
| BM 8 | | | 8.47 | 1124.92 | 1125.43 | Spike in root 12" Maple 28' Rt E Sta 59+40 |
| | 12.18 | 1144.74 | 0.83 | 1132.56 | | |
| | 13.30 | 1157.41 | 0.63 | 1144.11 | | |
| BM 9 | | | 3.31 | 1154.10 | 1154.61 | Spike in root 12" Maple 30' Rt E Sta 65+00 |
| | 12.41 | 1164.76 | 5.06 | 1152.35 | | |
| | 13.32 | 1177.69 | 0.39 | 1164.37 | | |
| BM 10 | | | 3.69 | 1174.00 | 1174.51 | Spike in root 12" Elm stump 20' Lt E Sta 70+80 |
| | 11.56 | 1188.88 | 0.67 | 1177.32 | | |
| BM 11 | 9.82 | 1187.09 | 11.61 | 1177.27 | 1177.78 | Spike in root 15" Maple 60' Rt E Sta 76+20 |
| | 9.25 | 1195.76 | 0.58 | 1186.51 | | |
| | 4.54 | 1199.83 | 0.47 | 1195.29 | | |
| BM 12 | | | 6.10 | 1193.73 | 1194.24 | Spike in root 20" Maple 60' Rt E Sta 83+60 |
| | 12.34 | 1206.69 | 3.70 | 1193.13 | | |
| | 6.89 | 1214.76 | 0.80 | 1207.87 | | |
| BM 13 | | | 5.77 | 1208.99 | 1209.50 | Spike in root 30" 4 twin Elm 30' Rt E 91+20 |
| | 11.62 | 1220.51 | 0.37 | 1213.37 | | |
| | 8.65 | 1233.34 | 0.82 | 1224.69 | | |

| | | | | | | corrected Elev. | |
|---|---|---|---|---|---|---|---|
| | | | 123334 | | | | |
| BM | 14 | 444 | 123638 | 140 | 123194 | 123245 | Spike in root 48' E Elm 50' Rt ℄ Sta 100+90 |
| | | 988 | 124443 | 183 | 123455 | | |
| | | 242 | 124493 | 192 | 124251 | | |
| TP | | | | 183 | 124310 | 124337 | = 12 Top IP Hyp. 36' Lt ℄ Sta 108+65 |
| | | 185 | 123579 | 1092 | 123394 | | |
| Sta 114 | | 253 | 123105 | 727 | 122852 | 122857 253 | |
| BM | 15 | 046 | 123372 | 779 | 122326 | 122377 | 2 spikes inside 6" Maple 30' Rt ℄ Sta 118+40 |
| | | 092 | 121218 | 1246 | 121126 | 935 | |
| | | -0.01 | 120274 | 945 | 120273 | | |
| | | 1.01 | 119272 | 1103 | 118171 | | |
| | | 1.16 | 118334 | 1054 | 118218 | | |
| BM | 16 | 3.92 | 117775 | 345 | 117830 | 117437 | Spike in root 18" Elm 25' Rt ℄ Sta 134+01 |
| | | 5.06 | 118004 | 280 | 117498 | | |
| | | 3.10 | 118034 | 280 | 117724 | | |
| BM | 17 | | | 11.93 | 116841 | 116892 | 2 spikes inside 24" Ash 45' Rt ℄ Sta 145+00 |
| BM | 18 | | | 6.12 | 117422 | 117473 | Spike in root 14" Maple 300' Lt ℄ Sta 145+50 = Sta 162+10 Chilliwack Road Imp. 25' Rt ℄ |

| | | | | Parks Elev | |
|---|---|---|---|---|---|
| BM 17 | 062 | 116254 | | 1168.92 | |
| | 078 | 115956 | 10.76 | 115878 | |
| BM #19 | | | 811 | 115145 | 11 |
| | 065 | 114833 | 1188 | 114768 | |
| | 072 | 113630 | 1275 | 113558 | |
| BM #20 | 933 | 113686 | 8.77 | 1127.53 | |
| | 10.71 | 1147.38 | 019 | 113667 | |
| | 6.66 | 115357 | 047 | 114691 | |
| | 105 | 114445 | 1017 | 114340 | |
| BM #21 | | | 069 | 1143.76 | |
| | 0.98 | 113670 | 8.73 | 113572 | |
| | 203 | 112948 | 925 | 112745 | |
| BM #22 | | | 3.93 | 1125.55 | |
| | 033 | 111920 | 10.61 | 111887 | |
| BM #23 | 026 | 110842 | 10.99 | 110821 | |
| | 0.90 | 119670 | 1269 | 109580 | |
| BM #24 | | | 1176 | 1084.24 | |

Spike in root 24" Maple 24' Rt ℄ Sta 150+01

Spike in root 20" Maple 25' Rt ℄ Sta 158+70

Spike in root 24" Elm 25' Lt ℄ Sta 168+40

S

Spike in root 20" Maple 35' Rt ℄ Sta 177+30

Spike in root 24" Apple 60 Lt ℄ Sta 183+30

X cut NE & NW edge nail 12' Lt ℄ Sta 189+30

| | | | | | Corrected Elev. | |
|---|---|---|---|---|---|---|
| BM #29 | 419 | 1089.13 | | 108494 | 108494 | X NE & N Headwall 12Lt & Sta 189+90 |
| | 1017 | 1098.96 | 036 | 108877 | | |
| BM #25 | 949 | 1101.35 | 210 | 107686 | 107686 | Spike in root 36" Elm 25 Lt & Sta 197+05 |
| | 277 | 1096.1 | 719 | 107416 | | |
| | 077 | 1085.17 | 1274 | 108420 | | |
| | 013 | 1072.46 | 1284 | 107233 | | |
| BM #26 | 950 | 1072.46 | 950 | 1082.96 | 1062.75 | Spike in root 8" Maple 35' Rt & Sta 207+50 |
| | 028 | 1059.96 | 1278 | 1059.68 | | |
| | 028 | 1047.48 | 1276 | 1047.20 | | (note: BM #27 2 spikes inside 6" Maple 50' Lt & Sta 211+50 Elev - 1036.37) |
| | 022 | 1034.20 | 1280 | 1034.68 | | |
| | 070 | 1023.26 | 1234 | 1022.76 | | |
| BM #28 | 200 | 1073.26 | 200 | 1021.26 | 1021.05 | Spike in root 24" Hickory 40' Rt & Sta 214+52 |
| | 058 | 1014.84 | 9.00 | 1014.26 | | |
| | 146 | 1007.84 | 846 | 1006.38 | | |
| BM #29 | 041 | 1007.84 | 041 | 1007.43 | 1007.22 | Spike in root 18" Ash 40' Rt & Sta 217+60 |
| | -005 | 1001.23 | 666 | 1001.18 | | (note: BM 30 = 2 spikes inside 8" Maple 40' Rt & Sta 226+50 Elev 990.76) |
| | 084 | 99317 | 870 | 992.33 | | |
| | 269 | 98604 | 782 | 983.35 | | |
| BM 31 | 364 | 98604 | 364 | 98240 | 982.19 | Spike in root 18" Maple 50' Rt & Sta 231+25 |

| | | | | | Corrected Elev | |
|---|---|---|---|---|---|---|
| | | 98609 | | | | |
| | 314 | 98302 | 616 | 97988 | | |
| | 270 | 976.52 | 220 | 97782 | | |
| BM#32 | 308 | 976.52 | 308 | 97344 | 973.23 | Spike in root 18" Ash 45' Rt & Sta 237+15 |
| | 142 | 971.56 | 638 | 97014 | | |
| | 115 | 966.59 | 612 | 96544 | | |
| | 354 | 96502 | 5.11 | 96148 | | |
| BM#33 | 953 | 96502 | 953 | 95549 | 955.28 | Spike in root 18" Willow 25' Rt & Sta 248+10 |
| | 682 | 962.35 | 249 | 96253 | | |
| BM#34 | 820 | 97572 | 233 | 96702 | 966.81 | Spike in root 6" Sycamore 36' Rt & Sta 255+50 |
| | 1197 | 98668 | 051 | 97471 | | |
| | 1200 | 99860 | 008 | 98660 | | |
| | 1140 | 1010.00 | 000 | 99860 | | |
| BM#35 | 278 | 1010.00 | 278 | 100722 | 1007.01 | Spike in side 10" Apple 28' Lt & Sta 261+40 |
| | 741 | 1010.72 | 1.69 | 100831 | | |
| BM#36 | | | 278 | 101494 | 1014.73 | Spike in root 24" Apple 20' Rt & Sta 265+55 |
| | | | | | | = Elev on Monson Imp 1014.83 |

BM-32

973.23

| | | | | |
|---|---|---|---|---|
| B.M. 22 | 3.88 | 1129.43 | | 1125.55 |
| 178 | | | 3.9 | 1125.5 |
| 178+60 | | | 4.4 | 1125.0 |
| 179 | | | 6.7 | 22.7 |
| 180 | | | 10.5 | 18.9 |
| | 0.62 | 1119.58 | 10.47 | 1118.26 |
| 181 | | | 2.5 | 17.1 |
| 182 | | | 7.5 | 12.1 |
| 183 | | | 12.6 | 07.0 |
| | 1.89 | 1108.42 | 13.05 | 1106.53 |
| B.M. 23 | 0.17 | 1108.38 | 0.17 | 1108.25 |
| 184 | | | 6.6 | 01.8 |
| 185 | | | 12.1 | 1096.3 |

(1125.53)

30/3.1 19/5.3 15/5.0 7/4.5 8/3.9 13/4.4 30/3.7

(1125.03)

30/2.8 18/2.9 14/4.0 7/4.7 8/4.4 9/4.7 10/4.9 16/2.8 30/2.7

(1122.73)

30/3.5 25/3.6 5/6.6 6.7 10/7.2 13/6.2 22/5.0 30/5.0

(1118.93)

30/9.0 16/9.3 11/11.2 9/11.8 5/10.8 10.5 10/10.7 30/12.5

(1117.08)

30/0.4 27/0.7 18/2.0 9/2.9 2.5 9/3.4 12/3.0 30/4.8

(1112.08)

30/2.2 20/2.7 8/7.6 6/7.3 7.5 6.5/7.6 8/8.0 11/8.7 15/5.1 30/6.4

(1106.98)

30/11.1 17/13.9 12/14.5 11/13.5 9/13.0 8/12.6 7.5/13.0 8.5/13.5 10/14.2 15/11.5 30/11.0

(1101.78)

30/6.2 15/5.9 10.5/8.2 10/7.2 6.6 7/7.3 10/8.0 16/4.5 30/4.2

(1096.28)

22/8.3 17/7.3 9.5/12.3 8/13.7 4.5/12.5 12.1 7/12.1 10.5/13.7 16/10.3 30/10.4

| | | | | | |
|---|---|---|---|---|---|
| | | 1108.38 | | | |
| | 0.37 | 1096.19 | 12.56 | 1095.82 | |
| 186 | | | 4.4 | 91.8 | |
| 187 | | | 7.3 | 88.9 | |
| 188 | | | 9.7 | 86.5 | |
| 189 | | | 11.2 | 85.0 | |
| BM #24 | 2.44 | 1087.38 | 11.17 | 1085.02 | 118494 |
| 189+90 | Stone Culvert | | 3.8 | 83.6 | |
| 190 | | | 4.4 | 83.0 | |
| 191 | | | 4.1 | 83.3 | |
| | 6.48 | 1091.17 | 2.69 | 1084.69 | |
| 191+50 | | | 7.7 | 83.5 | |
| 191+65 | | | 7.6 | 83.6 | |

(1091.79)

30 / 5.4 — 12 / 5.8 — 10.5 / 5.6 — 9 / 5.0 — 4 / 4.4 — 7.5 / 5.1 — 10 / 5.3 — 14.5 / 3.3 — 30 / 3.4

(1088.89)

30 / 8.2 — 15 / 8.2 — 11 / 8.9 — 7 / 7.5 — 7 / 7.3 — 5 / 7.8 — 9 / 8.6 — 11 / 8.2 — 30 / 8.3

(1086.49)

30 / 9.7 — 16 / 10.4 — 11 / 11.9 — 9.5 / 11.2 — 8 / 10.2 — 9.7 — 8 / 10.3 — 11 / 10.7 — 15 / 10.6 — 30 / 10.7

(1085.00)

30 / 13.1 — 19 / 13.0 — 13 / 12.5 — 11 / 12.7 — 8 / 11.8 — 11.2 — 14 / 12.4 — 30 / 12.8

Outlet Flow gard — 1079.4 — 1082.1 — (1083.58) — 1082.3 — 1079.2

100 / 10.4 — 30 / 9.8 — 7.6 — Fl / 8.0 G. F.L. — TO / 6.3 F.L. Tot. — 12.7 / 2.5 T.of H.W. — 11 / 3.6 B. Flow — 3.8 — 10 / 3.5 — 12.5 / 2.6 T. of H.W. — TO / 5.1 T.of G. — Fl / 8.2 F.L. — 30 / 7.9

(1088.00)

25 / 6.6 — 19.5 / 5.8 — 12 / 4.9 — 9 / 4.3 — 4.7 — 6 / 4.2 — 8.5 / 5.3 — 9.5 / 6.0 — 14 / 7.2 — 16 / 6.3 — 30 / 5.6

B. of C.

(1082.28)

30 / 6.7 — 20 / 6.0 — 13 / 5.1 — 12 / 5.7 — 10 / 4.9 — 4.1 — 5 / 4.8 — 6.5 / 5.2 — 8.5 / 4.8 — 11 / 4.3 — 30 / 5.0

(1083.47)

8 / 7.7 — 9 / 8.1 — 12 / 8.5 — 16 / 7.5 — 23 / 7.4 — 30 / 1.4 — 0.4

(1083.57)

100 / 12.1 — 30 / 12.8 — Fl / 10.0 F.L. — 21 / 9.2 T. of G. — 20 / 8.2 — 14.5 / 7.8 — 7.6 — 10 / 7.0 G — 11 / 7.4 T. of P. — Fl / 8.4 F.L. — 30 / 5.0 — 7.6 / 7.1

1081.2 — 1082.8

| | | | | | |
|---|---|---|---|---|---|
| | | 1091.17 | | | |
| 192 | | | 5.9 | 1085.3 | |
| | 11.06 | 1100.19 | 2.04 | 1089.13 | |
| 193 | | | 12.0 | 88.2 | |
| 194 | | | 8.9 | 91.3 | |
| 195 | | | 5.1 | 95.1 | |
| 196 | | | 4.4 | 95.8 | |
| 197 | | | 4.4 | 95.8 | |
| B.M 25 | 6.89 | 1103.75 | 3.31 | 1096.88 | 1096.86 |
| 198 | | | 7.7 | 96.1 | |
| 198+27 | V. Pipe Culvert | 181 | 8.0 | 95.8 | |
| 199 | | | 7.4 | 96.4 | |

(1085.27)

30/7.5 20/6.1 13/6.7 11/7.2 8/6.6 6/5.9 6/6.5 7/6.7 9/6.2 15/5.1 30/9.6

(1088.19)

30/10.8 20/10.6 16/10.5 12.5/11.0 9/13.2 7/12.7 5/12.1 5/12.9 6/13.8 8/12.6 12/10.8 17/9.1 30/8.6

(1091.29)

30/7.3 23/6.9 13/7.3 9/10.5 7.5/9.9 6/8.9 5.5/9.7 7.5/10.6 11/8.5 13/7.9 30/7.2

(1095.09)

30/4.9 21/4.1 12/4.9 10/6.5 8/6.0 6/5.1 5/6.0 7/6.8 10/5.3 16/4.4 30/3.6

(1095.29)

30/5.7 23/5.1 14/4.7 12.5/5.6 9/5.1 5/4.1 4/4.4 4/5.0 7/5.6 9/4.6 15/3.0 30/2.1

(1095.29)

30/3.9 15/3.9 10/4.6 6/4.4 6.5/5.1 8/5.0 12/5.3 30/2.6

(1096.05)

30/9.2 20/9.0 16/9.0 13/8.8 9/8.0 7/7.7 4/7.7 8/8.8 10/8.9 13/8.4 30/8.2

(1095.75)

60/10.9 50/9.7 11/9.0 8/8.8 6/7.9 8/8.0 7/7.6 10/8.4 5.4/9.2 50/8.5 100/7.7

Fl. grade 1094.6

(1096.35)

30/5.6 22/5.9 13/7.5 9/8.1 8/7.6 7.4 10/7.6 11/8.1 13/5.6 30/5.1

| | | | | |
|---|---|---|---|---|
| | | 1103.75 | | |
| 200 | | | 6.5 | 97.3 |
| 201 | | | 8.7 | 95.1 |
| 202 | | | 9.1 | 94.1 |
| | 2.43 | 1097.03 | 9.15 | 1094.60 |
| 203 | | | 3.3 | 93.7 |
| 203+40 | | | 1.9 | 92.1 |
| 204 | | | 9.4 | 87.4 |
| 204+30 | | | 11.5 | 85.5 |
| | 3.24 | 1087.26 | 13.01 | 1084.02 |
| 205 | | | 5.0 | 82.3 |
| 206 | | | 12.3 | 75.0 |
| 207 | | | | |

(1097.25)

30 19 11 10 6 7 8 13 30
4.8 4.9 6.1 5.9 6.4 6.5 6.5 6.6 6.2 6.3

(1095.05)

35 30 17 11 6 9 11 14 20 30
7.8 7.5 7.8 9.9 9.2 8.7 9.1 9.5 8.1 6.9 7.2

(1094.05)

30 13 11 10 11 19 30
8.9 10.2 10.5 10.1 9.7 10.4 10.7 11.4

1100.43

30 17 11 9 8 8 9 11 30
0.9 1.4 3.6 4.6 3.8 3.3 4.0 4.2 3.2 4.5

(1092.13)

30 15 11 8 7 8 13 30
2.4 2.4 6.5 5.3 4.9 5.1 5.6 3.3 4.7

(1087.43)

20 19 10 8 6 7.5 16 30
7.1 6.5 10.5 9.8 9.6 10.0 10.4 5.5 6.0

(1085.53)

30 16 11 9 6 7 11 13 30 35
10.0 10.2 12.6 12.1 11.5 11.8 10.3 10.7 9.3 9.4 8.3

(1082.26)

30 20 13.5 10.5 9 7 12 30
0.7 1.2 4.4 5.9 5.1 5.0 5.5 3.8 4.9

(1075.00)

45 40 30 26 10 8 4 5 10 30
1.9 2.1 3.4 4.6 13.0 12.5 12.3 12.9 10.7 9.1 11.9

45 40 30
4.2 3.6 13.9

| | | | | | |
|---|---|---|---|---|---|
| | | 1087.26 | | | |
| | 0.86 | 1075.31 | 12.75 | 1074.51 | |
| 207 | | | 8.8 | 66.6 | |
| 207+30 | | | 10.0 | 1065.4 | |
| | 3.47 | 1066.33 | 1251 | 1062.86 | |
| BM #26 | 3.56 | 1066.31 | 3.56 | 1062.77 | 1062.75 |
| 208+00 | | | 4.6 | 1061.7 | |
| 208+50 | | | 6.2 | 60.1 | |
| 209 | | | 11.4 | 54.9 | |
| BM #26 | | | 3.56 | 1062.75 | |

1066.51

165 135 11 3 4 10 30 35
8.2 9.8 8.7 8 8.9 7.7 6.4 10.0 11.5

50
1079.0

(1065.31)

43 31 12 13.5 11 5 10 20 30
1076.5 2.1 8.8 10.6 9.8 10.0 10.0 11.2 12.3 12.5

50
1072.4

(1061.21)

45 30 22 17 15 11 4.6 30
1077.2 1070.5 3.2 3.3 4.8 3.9 8.7

50 555
1074.4 1075.4

(1060.11)

40 30 25 17 16 7 4 18 30
1076.6 12 9.6 5.8 5.4 0.8 6.2 6.2 12.3 10.6

50
1068.6

(1054.91)

40 35 30 25 6 5 12 30
1062.3 0.9 2.2 1.5 11.0 10.5 11.7 10.2 13.3

| | | | | |
|---|---|---|---|---|
| B.M.#26 | 2.36 | 1065.11 | | 1062.75 |
| 209+25 | | | 12.3 | 52.8 |
| | 1.55 | 1054.58 | 12.08 | 1053.03 |
| 209+50 | | | | 50.2 |
| 209+80 | | | | 48.5 |
| 210 | | | | 47.0 |
| 210+25 | | | | 45.3 |
| 210+65 | | | | 41.9 |
| | 3.76 | 1045.93 | 12.91 | 1042.17 |
| 211 | | | 7.4 | 38.5 |
| B.M.#27 | | | 9.56 | 1036.37 |
| 211+25 | | | 10.5 | 35.4 |

(1052.81)

(1050.18)

(1047.00)

(1038.53)

1 2" Horiz. Spikes in 6" Maple 50'L+R Sta. 211+50

| | | | | |
|---|---|---|---|---|
| | | 1045.93 | | |
| 211+70 | | | | |
| 212+20 | | | | |
| | 3.01 | 1037.81 | 11.13 | 1034.80 |
| 211+70 | | | 8.0 | 29.8 |
| 211+80 | | | 5.8 | 32.0 |
| 212+20 | | | 5.4 | 32.4 |
| 212+50 | | | 8.6 | 29.2 |
| 212+60 | | | 11.1 | 26.7 |
| | 2.19 | 1027.01 | 12.99 | 1024.82 |
| 212+50 | | | | |
| 212+60 | | | | |
| 212+70 | Creek | | 8.1 | 18.7 |
| 212+75 | W. Bank - N | | 8.1 | 18.9 |

50

— 34/13.3 48/4.5 64/1051.7 80/1064.9

— 55/12.3 59/8.4 67/3.8 80/2.9

48/1.7 36/3.5 245/5.3 10/7.5 —/8.0 1.5/3.2 3/6.7 7/6.7 10.5/7.8 13/7.4 29/7.1 27/8.6 30/6.0

47/0.2

45/1.6 27/2.6 11/2.1 —/5.8 5/8.8 8/8.8 11/7.9 26.5/7.7 30/9.5 32.5/9.4 40/4.3

(1032.41)

50/3.6 25/2.9 12/2.9 —/5.4 14/12.3 12.5/11.3 36/11.2 38/12.9 41/12.9 44/11.2 48/10.8

32/5.1 24/4.0 18/5.4 9/8.9 —/8.6 8.5/8.0 15.5/12.0 —

30/5.1 26/5.1 21/6.1 2/11.3 —/11.1 11/13.2

75/3.3 67/1.6 60/3.6 47/4.2

— 17/2.2 18-19/3.1 21/2.0 35/2.1 38/5.1 42-46/5.7

50/2.0 Stream

15/3.0 17-19/3.8 21/2.3 33/2.2 38/5.2 41/6.5

N 9 End

30/8.8 —/8.1 21—Bldg 7.7-2.3 Bldg 2.4 35/7.4 50/7.0 70/6.9 100/5.5

30/2.7 23/4.9 8.0/3.6

| | | | | | |
|---|---|---|---|---|---|
| | | 1022.01 | | | |
| 212+80 | | | 6.7 | 20.3 | |
| C13 | | | 6.5 | 20.5 | |
| 214 | | | 7.7 | 19.3 | |
| BM#28 | 1.51 | 1022.56 | 5.95 | 10 21.06 | 1021.05 |
| 214+60 | | | 4.5 | 18.1 | |
| 215 | | | 5.4 | 17.2 | |
| BM#27 | | | | | |
| | | | 1.51 | 1021.05 | |

6 7 $\frac{18}{5.3}$ $\frac{22}{3.8}$ $\frac{32}{3.7}$ $\frac{36}{5.4}$ $\frac{40}{6.2}$

(1020.51)

Channel $\frac{36}{8.8}$ $\frac{25}{7.3}$ $\frac{18}{6.5}$ $\frac{11}{6.1}$ $\frac{}{6}$ $\frac{9}{5.5}$ $\frac{16}{5.0}$ $\frac{22}{5.3}$ $\frac{32}{4.0}$ $\frac{40}{3.5}$ $\frac{50}{3.6}$

(1019.31)

Channel $\frac{37}{9.9}$ $\frac{30}{9.2}$ $\frac{23}{8.7}$ $\frac{16}{7.2}$ $\frac{6}{7.0}$ $\frac{3}{7.9}$ $\frac{}{7}$ $\frac{35}{7.5}$ $\frac{11}{7.9}$ $\frac{17}{5.6}$ $\frac{30}{5.2}$ $\frac{50}{4.8}$

Channel

$\frac{30}{5.5}$ $\frac{24}{5.9}$ $\frac{21}{6.}$ $\frac{14}{7.3}$ $\frac{11}{4.1}$ $\frac{4}{3.8}$ $\frac{3}{4.5}$ $\frac{}{5}$ $\frac{9}{4.2}$ $\frac{10}{4.6}$ $\frac{13}{3.9}$ $\frac{25}{3.7}$ $\frac{30}{4.4}$

$\frac{55}{7.6}$ stream

(1017.16)

Stream

$\frac{45}{6.6}$ $\frac{30}{6.4}$ $\frac{21}{7.0}$ $\frac{24}{7.0}$ $\frac{22}{6.1}$ $\frac{9}{6.4}$ $\frac{4}{4.6}$ $\frac{}{5}$ $\frac{9}{4.9}$ $\frac{10.5}{5.3}$ $\frac{13}{4.3}$ $\frac{21}{3.7}$ $\frac{30}{3.7}$

16.0 16.2 15.6 15.6 16.5 16.2 18.0 17.7 17.3 18.3 18.9 18.9

| | | | | | |
|---|---|---|---|---|---|
| BM #28 | 0.53 | 1021.58 | | 1021.05 | |
| 215+50 | | | 5.4 | 1016.2 | |
| | | | 1015.08 | | |
| 216 | | | 6.5 | 1015.1 | |
| | | | 1011.58 | | |
| 217 | | | 10.0 | 1011.6 | |
| | 1.36 | 1012.10 | 10.84 | 1011.74 | |
| | | | 1008.66 | | |
| 218 | | | 3.5 | 1008.6 | |
| | | | 1006.00 | | |
| 219 | | | 6.1 | 1006.0 | |
| | | | 1004.40 | | |
| 219+50 | | | 7.7 | 1004.4 | |
| BM #29 | 4.89 | 1012.11 | 4.89 | 1007.22 | 1007.22 |
| | | | 1003.41 | | |
| 220 | | | 8.7 | 1003.4 | |
| | 1.38 | 1004.27 | 2.22 | 1002.89 | |
| | | | 1002.42 | | |
| 221 | | | 2.0 | 1002.3 | |
| 221+50 | | | 2.7 | 1001.6 | |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| | 24 / 62 | 20 / 83 | 12-10 / 82 | 8 / 75 | 4 / 53 | 5 / 52 | 7 / 54 | 9 / 53 | 12 / 41 | 20 / 32 | 30 / 29 |
| | 15.1 | 13.3 | 13.4 | 17.1 | 16.3 | 16.4 | 16.2 | 16.6 | 17.5 | 14.4 | 18.7 |
| | 30 / 65 | 26 / 49 | 15 / 48 | 10 / 65 | 3 / 63 | 2 / 69 | 4.5 / 66 | 7 / 58 | 14 / 53 | 30 / 50 | |
| | 15.1 | 16.7 | 16.8 | 15.1 | 15.3 | 15.2 | 15.0 | 15.8 | 16.3 | 16.6 | |
| 20 channel 11.5 | | 30 / 97 | 27 / 89 | 12 / 83 | 8 / 10.0 | 7 / 99 | 17 / 79 | 30 / 70 | — | | |
| | | 11.9 | 12.7 | 13.3 | 11.6 | 11.7 | 14.3 | 14.6 | | | |
| 55 channel 4.3 | | 30 / 26 | 23 / 23 | 7 / 23 | 9 / 31 | 5 / 29 | 11 / 31 | 17 / 07 | 33 / 03 | 30 / 05 | |
| | | 9.5 | 9.8 | 9.8 | 9.0 | 09.2 | 9.0 | 11.4 | 11.9 | 11.6 | |
| | 30 / 41 | 17 / 32 | 10 / 32 | 4-3 / 7.1 | 15 / 62 | 6 / 67 | 11 / 65 | 13 / 46 | 18 / 43 | 28- / 67 | |
| | | 30 / 57 | 13 / 34 | 6-5 / 72 | 9 / 74 | 10 / 80 | 13-6 / 68 | 18 / 78 | 30 / 76 | | |
| | | 30 / 68 | 19 / 63 | 9.5 / 70 | 5. / 86 | 9 / 83 | 13 / 72 | 17-7 / 66 | 13 / 81 | 30 / 80 | |
| | | 32 / 1.8 | 4 / 1.4 | 3 / 24 | 1.5 / 1.9 | 2.0 | 13 / 2.0 | 15.5-16 / 0.6 | 20.5 / 2.2 | 30 / 2.1 | |
| | | 30 / 3.2 | 6 / 2.1 | 4 / 3.0 | 3 / 2.6 | 9 / 2.6 | 11 / 2.8 | 15 / 1.6 | 18 / 2.7 | 30 / 27 | 27 / 1016 / 0.76 |

| | | | | | |
|---|---|---|---|---|---|
| 221+75 | | 1004.27<br>3.8<br>0.5 | 1001.27<br>3.0 | 1001.3 | $\frac{30}{3.4}$ $\frac{16}{3.2}$ $\frac{5.5}{2.4}$ $\frac{3}{3.4}$ $\frac{6}{3.0}$ $\frac{10}{2.7}$ $\frac{11}{3.1}$ $\frac{18}{0.0}$ $\frac{30}{10\ 8.1}$ $\frac{45}{18\ 13.6}$ |
| 221+90 | | | | | $\frac{100}{6.6}$ $\frac{30}{5.3}$ $\frac{Fl}{4.3}$ $\frac{Fl.}{3.8}$ |
| 222 | | | 1000.27<br>3.9 | 1000.4 | $\frac{30}{3.8}$ $\frac{20}{3.8}$ $\frac{15}{3.2}$ $\frac{11}{4.4}$ $\frac{6.5}{3.6}$ $\frac{11}{2.8}$ $\frac{22}{2.7}$ $\frac{27}{2.0}$ $\frac{30}{0.5}$ |
| 222+74. | | | 5.6 | 998.7 | $\frac{100}{7.6}$ $\frac{100}{7.7}$ $\frac{30}{6.5}$ $\frac{30}{2.8}$ |
| 222+74 | 120 Ft.<br>Left of ℄ | | | | $\frac{Fl.West}{11.5}$ |
| 223 | | | 997.87<br>6.4 | 997.9 | $\frac{30}{6.7}$ $\frac{22}{6.4}$ $\frac{14.5}{7.2}$ $\frac{12}{8.6}$ $\frac{10.5}{7.5}$ $\frac{7.5}{5.6}$ $\frac{9.5}{6.3}$ $\frac{13}{4.7}$ $\frac{30}{3.3}$ |
| 223+65 | | | 9.0 | 995.3 | $\frac{30}{7.9}$ $\frac{20}{7.7}$ $\frac{16}{8.3}$ $\frac{14}{9.9}$ $\frac{12.5}{9.6}$ $\frac{2.5}{9.1}$ $\frac{4}{9.6}$ $\frac{7}{6.6}$ $\frac{12}{4.4}$ $\frac{15}{5.3}$ $\frac{18}{4.5}$ $\frac{30}{3.7}$ |
| 224 | | | 994.27<br>10.0 | 994.3 | $\frac{30}{10.3}$ $\frac{20}{[illegible]}$ $\frac{16}{8.5}$ $\frac{13.5}{9.5}$ $\frac{12}{10.6}$ $\frac{4}{9.7}$ $\frac{6}{10.5}$ $\frac{9}{8.9}$ $\frac{17}{8.0}$ $\frac{28-30}{3.5}$ |
| 222+74 | 12.42 | 1016.69 | 0.00 | 1004.27 | $\frac{100}{7.3}$ $\frac{150}{1.8}$ $\frac{160}{0.0}$ |
| | 1.51 | 995.28 | 10.50 | 993.77 | |

| | | | | | |
|---|---|---|---|---|---|
| | 995.28 | | | | |
| 224+20 | | 993.78<br>1.5 | 993.8 | | |
| 224+85 | | 2.9 | 992.4 | | |
| 225 | | 992.28<br>3.0 | 992.3 | | |
| 225+75 | | 4.9 | 990.4 | | |
| 226 | | 989.58<br>5.7 | 989.6 | | |
| 226+25 | | 6.3 | 989.0 | | |
| 227 | | 986.88<br>8.4 | 986.9 | corrected elev | |
| BM #30 | | 4.56 | 990.72 | 990.76 | |
| 227+43 | Culvert | 8.1 | 987.2 | | |
| 227+85 | | 983.58<br>11.7 | 983.6 | | |

994.5 9949 L 2.0 13 3.7 11 2.1 45 1.0 9 1.9 12 0.3 26 0.0 30 993.8

31 9963 15 9963 13 5.0 8 2.4 7 2.2 5 3.2 9 2.2 13 1.2 30 1.0

30 99

30-25 9948 17 995 7/5 0.0 6 3.3 7 2.4 9 3.2 16.5 2.4 14.5 0.5 18 996.0

Chan. 8.6 30 4.4 20-16 2.8 12-10 4.7 7-4 5.8 7 4.9 5 5.5 12.5 7.0 17 996.1 30 9938

30 3.6 17 3.5 13-10 5.0 8-5 5.2 6.1 7 5.2 9 5.9 10-11 5.4 16 2.8 30 0.0

31 7.3 17 6.9 16 5.3 11 5.5 9-7 6.0 7 6.0 8.5 6.4 9.5 5.8 13 9.9 30 4.9

30 8.6 15.5 5.0 14 8.5 8 7.4 8 7.6 9 7.9 10 7.0 25 7.2 30 7.4

2 Shots N. side 8' Mard = 90' Rt. Sta 226+50

30 10.2 FL 11.7 TL 8.9 HW 6.9 GL 7.3 GR. 8.0 HW 7.1 T.L. 9.2 FL 11.1 43.6 48 Sa 10.5 25 11.2 125 12.0

30 8.9 22 9.4 18.5 10.5 11 11.0 8 11.3 5 16.3 10 10.4 15 10.0 30 10.2

228+60 Same as 227+85

| | | | | | | |
|---|---|---|---|---|---|---|
| | | 995.28 | | | | |
| | 2.48 | 987.49 | 10.27 | 985.01 | | |
| 228+75 | | | 4.5 | 983.0 | | $\frac{30}{4.1}$ $\frac{18}{3.7}$ $\frac{10-7}{4.7}$ $\frac{12}{4.1}$ $\frac{14}{3.5}$ $\frac{18}{2.9}$ $\frac{20}{7.0}$ $\frac{24}{7.0}$ $\frac{30}{5.2}$ $\frac{45}{4.0}$ |
| 229 | | | 982.59<br>4.9 | 982.6 | | $\frac{30}{5.4}$ $\frac{20}{6.1}$ $\frac{12-13.5}{4.3}$ $\frac{9}{5.3}$ $\frac{7}{4.8}$ $\frac{5}{4.9}$ $\frac{10}{5.1}$ $\frac{13.5-17.5}{3.9}$ $\frac{24}{4.6}$ $\frac{30}{4.8}$ |
| 230 | | | 981.69<br>5.8 | 981.7 | | $\frac{30}{6.2}$ $\frac{15}{6.2}$ $\frac{10}{6.2}$ $\frac{8-7}{6.5}$ $\frac{3}{5.6}$ $\frac{8}{5.8}$ $\frac{10}{6.1}$ $\frac{16}{5.8}$ $\frac{30}{6.2}$ |
| 231 | | | 981.38<br>6.7 | 980.8 | | $\frac{30}{6.7}$ $\frac{9}{6.0}$ $\frac{4.5}{7.0}$ $\frac{3}{6.8}$ $\frac{4}{6.7}$ $\frac{6-8}{6.2}$ $\frac{12}{7.0}$ $\frac{15}{6.5}$ $\frac{30}{6.7}$ |
| BM# 31 | 5.42 | 987.61 | 5.42 | 982.07 | 982.19 | $\frac{125}{13.0}$ $\frac{200}{974.0}$ 231+40 same as 231 |
| 231+30 | Culvert | | 6.5 | 981.1 | | $\frac{100}{12.2}$ $\frac{50}{11.9}$ $\frac{20}{11.9}$ $\frac{EL}{11.6}$ $\frac{TI}{7.7}$ $\frac{HW}{5.5}$ $\frac{Gr}{6.5}$ $\frac{Gr}{6.3}$ $\frac{HW}{5.3}$ $\frac{TI}{7.3}$ $\frac{FL}{11.0}$ $\frac{30}{10.5}$ |
| | | | | | | 976.0 976.0 |
| 231+65 | | | 7.8 | 979.8 | | [illegible] $\frac{33}{11.5}$ $\frac{21}{10.1}$ $\frac{18}{7.3}$ $\frac{14}{7.4}$ $\frac{12}{7.6}$ $\frac{17}{4.2}$ $\frac{23}{0.0}$ $\frac{30}{991.5}$ $\frac{40}{998.5}$ $\frac{50}{1000.5}$ |
| | | | | | | 976.1 |
| | | | 5.42 | 982.19 | | |
| BM# 31 | 285 | 985.04 | | | 982.19 | |
| 232 | | | 979.54<br>5.5 | 979.5 | | $\frac{30}{58}$ $\frac{12}{56}$ $\frac{10-8}{59}$ $\frac{7}{55}$ $\frac{3}{55}$ $\frac{11}{57}$ $\frac{22}{52}$ $\frac{27}{33}$ $\frac{4.1}{997.0}$ 1:1+ |
| 233 | | | 978.44<br>66 | 978.4 | | $\frac{30}{69}$ $\frac{18}{64}$ $\frac{14-13}{7.1}$ $\frac{10-5}{62}$ $\frac{14}{6.7}$ $\frac{25}{58}$ $\frac{37}{0.2}$ — |
| 234 | | | 976.94<br>81 | 976.9 | | $\frac{30}{82}$ $\frac{18}{78}$ $\frac{14}{21}$ $\frac{13}{82}$ $\frac{2}{81}$ $\frac{5-7}{88}$ $\frac{10}{79}$ $\frac{21}{6.9}$ $\frac{30}{08}$ 1:1 up |

| | | | | | |
|---|---|---|---|---|---|
| | | 985.04 | | | |
| | 171 | 978.68 | 8.07 | 976.97 | |
| 234+90 | | | 36 | 975.1 | |
| 235 | | | 984.58 4.1 | 974.6 | |
| 236 | | | 972.68 6.0 | 72.7 | |
| 237 | | | 971.78 6.9 | 71.8 | |
| BM#32 | | | 5.45 | 973.23 | 973.23 |
| 238 | | | 971.00 7.7 | 71.0 | |
| BM#32 | 045 | 973.68 | | 973.23 | |
| 239 | | | 970.25 3.4 | 70.3 | |
| 239+55 | | | 3.5 | 70.2 | |
| 239+85 | | | 3.1 | 70.6 | |
| 240+50 | | | 970.15 3.5 | 70.2 | |

30 chain FS

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| | 60 65 | 30 47 | FL 74 | TO 36 | TO 36 | FL 45 | | | |
| | | | 974.3 | | | 974.2 | | | |
| — | 30 44 | | 10 36 | 8 43 | 3 41 | 5 32 | 20-30 25 | | |
| | 30 93 | 12 93 | 13-9 47 | 5-3 56 | 6 55 | 14 56 | 20 5.0 | 30 52 | |
| | 236+90 same as 236 level all left | | | | | | | | |
| — | 30 70 | | 20 61 | 9 65 | 2-6 64 | 9-10 68 | 13 63 | 30 61 | |
| — | 30 80 | | 14 78 | 10-2 71 | 23 84 | 30 82 | — | — | |
| | 30 46 | 17 46 | 14 31 | 4 30 | 28-35 44 | | — | — | |
| | 239+46 same as 239 | | | | | | | | |
| | 100 86 | 60 61 | FL 51 | TO 45 | TO 44 | FL 50 | 3 | | |
| | | | 63.6 | | 968.7 | | | | |
| — | 30 49 | | 19 45 | 9 32 | 5 28 | 10 0.0 | 21 977.7 | 40 980.7 | |
| — | 30 56 | | 14 90 | 9 42 | 7 28 | 16 00 | 22 974.1 | 36 978.1 | 42 977.2 |

| | | | | | |
|---|---|---|---|---|---|
| | | 97368 | | | |
| 241 | | | 968.05<br>5.6 | 68.1 | Top stake Lt x41+50' |
| | 1.69 | 969.75 | 5.62 | 968.06 | |
| 242. | | | 966.00<br>3.8 | 66.0 | |
| 243 | | | 965.00<br>4.8 | 65.0 | |
| 244 | | | 964.45<br>5.3 | 64.5 | |
| 244+96 | | | | | |
| 245 | | | 964.75<br>5.0 | 64.8 | |
| | 1.66 | 965.55 | 5.86 | 963.89 | |
| 246 | | | 961.95<br>3.8 | 61.8 | |
| 247 | | | 960.35<br>5.2 | 60.4 | |
| 247+85 | | | 5.4 | 60.2 | |
| Seat SW | | | 6.5 | 59.1 | |
| " NW | | | 6.0 | 59.6 | |

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| — | — | 30/65 | 5/58 | 5/54 | 13/44 | 22/972.6 | 28-30/973.7 | | 40/976.5 | |
| — | — | — | 30/37 | 4/3.6 | 14 | 18-21/4.1 | | 34/3.4 | 30/2.8 | |
| | 30/60 | 8/58 | 6/52 | 6/48 | 16/35 | 30/51 | — | | | |
| — | — | 30/59 | 1/50 | 15/57 | 8-10/44 | 12/32 | 25-30/34 | | | |
| | 275/1740 | 225/973 | 150/33 | 100/5.3 | | | | | | |
| 30/55 | 21/51 | 20/66 | 13/67 | 7/69 | 4/66 | 30/44 | — | — | | |
| 30/39 | 12/37 | 17/41 | 11/37 | 7-9/41 | 3/38 | 4/42 | 14/24 | 30/1.8 | | |
| — | 30/55 | 8-9/47 | 6/45 | 3/49 | 9/62 | 16/58 | 30/50 | | | |

247+50 same as 247 except 30/20 Left

| | | | | |
|---|---|---|---|---|
| | 965.55 | | | |
| | | 961.15 | | |
| E 248+19 | | 4.4 | 961.2 | |
| Scat SE | | 5.3 | 60.3 | |
| " NE | | 5.4 | 60.2 | |
| Flow W | | 17.6 | 48.0 | |
| BM #33 | | 10.26 | 955.29 | 955.28 |
| Flow E | | 17.4 | 48.2 | |
| Flow E | | 12.0 | 53.6 | |
| 248+30 | | 45 | 61.1 | |
| | | | | |
| | | 959.95 | | |
| 249 | | 5.6 | 60.0 | |

$\frac{50}{11.2}$ $\frac{-30}{55.5}$ $\frac{17}{102}$ $\frac{55}{45}$ $\frac{7}{48}$ $\frac{17}{89}$ $\frac{24}{103}$ $\frac{34}{158}$ $\frac{-50}{108}$

55.5 61.2 60.9 56.8 55.4 49.9

$-\frac{30}{10.0}$ $\frac{2}{91}$ $\frac{4}{57}$ $\frac{3}{53}$ $\frac{10}{56}$ $\frac{18}{10.2}$ $\frac{27}{165}$ $\frac{-40}{125}$

$\frac{59}{48}$
11

| | | | | |
|---|---|---|---|---|
| BM #33 | 9.70 | 964.98 | | 955.28 |
| 249+60 | | | 5.2 | 59.8 |
| 250 | | | 960.08<br>4.9 | 60.1 |
| | 6.33 | 966.99 | 4.32 | 960.66 |
| 251 | | | 961.08<br>5.9 | 61.1 |
| 251+50 | | | 961.39<br>5.6 | 61.4 |
| 252 | | | 961.99<br>5.0 | 62.0 |
| 253 | | | 963.39<br>3.6 | 63.4 |
| 253+75 | | | 2.6 | 64.4 |
| 254 | | | 964.79<br>2.2 | 64.8 |
| 254+30 | | | 1.8 | 65.2 |

30/8.5 20/7.6 11/7.0 9-3/5.0 2-9/4.7 6.5/5.1 9/5.0 11.5/5.5 27/5.5 37/14.4 43-35/15.4

30/6.0 15/5.7 12-9/6.5 7/5.9 3/4.8 2.5-3.5/4.5 5.5/5.0 8/4.7 12/5.9 22/6.2 38/6.1

30/8.0 18/7.2 15/7.3 13/6.9 35/5.3 7.5/6.6 10/6.5 12/6.9 14.5/6.6 21/7.1 30/7.2

30/4.2 19/4.2 12/4.5 9.5/5.7 2/5.3 5.5/5.9 13/6.0 17.5/5.0 23/4.8 26/9.4 30/9.8

30/3.1 19/2.6 12/2.1 9/5.1 5/5.3 11/5.4 21/2.1 26/2.1 30/2.5

30/3.6 12.5/3.6 8.5/3.1 7/3.9 2/4.1 4-7/4.0 15/3.5 20/3.6 24/3.7 30/3.8

30/2.0 8/2.3 6/3.0 5/3.0 10/3.1 16/3.6 23/5.2 30/5.2

30/1.7 22/1.6 11/2.0 6.5/2.7 9/2.8 8/2.6 14/2.3 23-30/5.8

30/1.9 21/1.6 11/1.7 7/2.3 4/2.4 8/2.2 13/0.9 20/0.4 30/1.4

| | | | | | | |
|---|---|---|---|---|---|---|
| | | 966.99 | | | | |
| | 6.41 | 973.29 | 0.61 | 966.38 | | |
| 255 | | | 966.29<br>7.0 | 66.3 | | $\frac{30}{7.0}$ $\frac{12}{7.7}$ $\frac{0}{7.7}$ $\frac{5-9}{7.5}$ $\frac{15}{7.2}$ $\frac{20}{6.6}$ $\frac{30}{7.0}$ |
| 255+65 | | | 6.0 | 67.3 | | $\frac{30}{7.1}$ $\frac{11}{6.9}$ $\frac{6.5}{6.3}$ $\frac{3}{6.4}$ $\frac{8}{6.5}$ $\frac{19}{6.7}$ $\frac{30}{10.9}$ |
| BM$^{\#}$34 | 6.42 | 973.23 | 6.42 | 966.87 | 966.81 | |
| 256 | | | 968.23<br>5.0 | 68.2 | | $\frac{30}{6.0}$ $\frac{23}{6.4}$ $\frac{20.5}{6.0}$ $\frac{12}{6.0}$ $\frac{8}{5.2}$ $\frac{6}{5.5}$ $\frac{2}{5.6}$ $\frac{8.5}{5.7}$ $\frac{19}{6.2}$ $\frac{30}{10.2}$ $\frac{35}{10.7}$ |
| 257 | | | 970.33<br>2.9 | 70.3 | | $\frac{30}{3.8}$ $\frac{18}{3.5}$ $\frac{12}{2.8}$ $\frac{6}{2.5}$ $\frac{3}{3.0}$ $\frac{5}{2.4}$ $\frac{7}{2.8}$ $\frac{11}{2.6}$ $\frac{14}{3.1}$ $\frac{16}{2.7}$ $\frac{25}{3.6}$ $\frac{30}{4.7}$ |
| | 12.54 | 985.16 | 0.61 | 972.62 | | |
| 257+50 | | | 12.6 | 72.6 | | $\frac{30}{10.0}$ $\frac{11}{11.5}$ $\frac{5.5}{12.1}$ $\frac{5}{13.4}$ $\frac{11}{12.2}$ $\frac{14}{12.8}$ $\frac{15-19}{12.1}$ $\frac{30}{13.1}$ |
| 258 | | | 976.56<br>8.6 | 76.6 | | $\frac{30}{3.2}$ $\frac{18}{3.9}$ $\frac{9}{10.1}$ $\frac{6}{9.1}$ $\frac{6}{8.8}$ $\frac{9}{9.9}$ $\frac{14}{7.0}$ $\frac{30}{7.5}$ |
| | 12.99 | 997.77 | 0.38 | 984.78 | | |
| 258+80 | | | 13.5 | 84.3 | | $\frac{30}{6.7}$ $\frac{18}{7.6}$ $\frac{10}{14.6}$ $\frac{7}{13.5}$ $\frac{5}{13.8}$ $\frac{7}{14.8}$ $\frac{14}{9.7}$ $\frac{20}{10.3}$ $\frac{30}{12.9}$ |
| 259 | | | 986.27<br>11.5 | 86.3 | | $\frac{30}{6.1}$ $\frac{19}{6.6}$ $\frac{11}{12.9}$ $\frac{8}{11.6}$ $\frac{2-4}{12.0}$ $\frac{6.5}{12.5}$ $\frac{13}{7.5}$ $\frac{19}{7.5}$ $\frac{30}{11.2}$ |
| | 11.50 | 1004.45 | 0.72 | 996.95 | | |
| 260 | | | 995.25<br>13.2 | 95.3 | | $\frac{30}{10.2}$ $\frac{16}{11.2}$ $\frac{11}{14.7}$ $\frac{7}{13.6}$ $\frac{6}{13.4}$ $\frac{11}{14.4}$ $\frac{13.5}{12.9}$ $\frac{20}{12.7}$ $\frac{30}{13.5}$ |

| | | | | | |
|---|---|---|---|---|---|
| | | 1008.45 | | | |
| 261 | | | 1003.05<br>5.4 | 1003.1 | |
| B.M.# 35 | 1.41 | 1008.42 | 1.41 | 1007.04 | 1007.01 |
| 261+35 | | | 3.5 | 1004.9 | |
| 262 | | | 1006.06<br>2.5 | 05.9 | |
| B.M.# 35 | 9.44 | 1016.45 | | | 1007.01 |
| 263 | | | 999.12<br>9.3 | 07.2 | |
| 264 | | | 1008.65<br>7.8 | 08.7 | |
| 265 | | | 1011.35<br>5.1 | 11.4 | |
| 265+36.7 | | | 1012.00<br>4.5 | 12.0 | |
| | Profile | East | | | |
| B.M.# 36 | | | 1.71 | 1014.74 | 1014.73 |

$\frac{38}{3.2}$ $\frac{18}{3.1}$ $\frac{5.5}{6.5}$ $\frac{2}{5.6}$ $\frac{9}{5.7}$ $\frac{13}{6.7}$ $\frac{16.5}{3.3}$ $\frac{30}{3.7}$ $\frac{44}{3.5}$

$\frac{30}{2.6}$ $\frac{9}{1.8}$ $\frac{2.5}{4.1}$ $\frac{11}{3.2}$ $\frac{16}{4.4}$ $\frac{18.5}{1.9}$ $\frac{30}{2.0}$

$\frac{30}{4.4}$ $\frac{5}{3.6}$ $\frac{1.5}{2.1}$ $\frac{7}{1.8}$ $\frac{12}{2.3}$ $\frac{13.5}{2.2}$ $\frac{16}{2.1}$ $\frac{30}{2.5}$

$\frac{30}{8.4}$ $\frac{18}{9.0}$ $\frac{10}{8.8}$ $\frac{4}{9.3}$ $\frac{6}{8.7}$ $\frac{13}{9.5}$ $\frac{30}{9.7}$

$\frac{30}{7.4}$ $\frac{22}{6.8}$ $\frac{10}{6.6}$ $\frac{4}{7.4}$ $\frac{3}{8.2}$ $\frac{1.5}{7.7}$ $\frac{5}{7.3}$ $\frac{10}{8.1}$ $\frac{12}{6.4}$ $\frac{30}{5.7}$

$\frac{30}{5.3}$ $\frac{9}{4.6}$ $\frac{6}{5.8}$ $\frac{3}{5.1}$ $\frac{9}{5.0}$ $\frac{12}{5.3}$ $\frac{18}{4.1}$ $\frac{30}{3.6}$

$\frac{30}{4.1}$ $\frac{25}{3.6}$ $\frac{17}{4.1}$ $\frac{15-19}{5.7}$ $\frac{11.5}{4.5}$ $\frac{30}{3.8}$ $\frac{50}{3.1}$ $\frac{100}{3.9}$ $\frac{200}{4.8}$ $\frac{250}{10.6}$

$\frac{50}{3.3}$ $\frac{100}{2.2}$ $\frac{150}{1.4}$ $\frac{200}{0.5}$

# Cross Sections after Storm

R Goodrich

| | | | | | |
|---|---|---|---|---|---|
| BM# 28 | 4.52 | 0.25,57 | | | 1021.05 |
| 212+90 | | | 4.1 | 1021.5 | |
| 213 | | | 5.0 | 1020.6 | |
| 213+50 | | | 4.8 | 1020.8 | |
| 214+60 | | | 7.7 | 1017.9 | |
| | 4.34 | 1021.73 | 8.18 | 1017.39 | |
| 215 | | | 4.7 | 1017.0 | |
| 215+50 | | | 6.0 | 1015.7 | |
| 215+80 | | | 6.4 | 1015.3 | |
| +83 | | | 6.7 | 1015.0 | |
| 216 | | | 7.5 | 1014.2 | |
| T.P | 3.55 | 1016.66 | 8.62 | 1013.11 | |



channel 120 15 10 17 22 30
7.8 5.8 4.5 3.3 3.6 3.5
17.7 19.8 21.1 22.3 22.0 22.1

25 22 12 6 16 18 27 30
7.6 6.2 4.5 4.0 3.6 4.8 4.6 3.3
18.0 19.4 21.1 21.6 22.0 20.8 21.0 22.3

23 12 5 6 11 16 19 22 30
6.5 3.5 3.7 5.1 5.7 8.0 5.1 3.7 2.8

12 11 4 7 7 11 13
8.5 7.1 6.7 7.5 7.2 7.6 6.9
17.1 18.6 18.9 18.1 18.6 18.0 18.7

21 17 7 4 2 7 9 12 19 20 30
5.9 5.1 5.4 3.6 4.0 4.5 4.1 4.3 3.4 3.0 3.0
15.8 16.6 16.7 18.1 17.7 17.2 17.6 17.4 18.3 18.7 18.7

19 13- 10 7 6 7-10 19 17 20 30
7.0 8.2 4.8 5.7 5.4 4.2 4.0 3.5 3.1
14.7 13.5 16.9 16.0 16.3 17.5 17.7 18.2

22 15 8 5 5 6 8
5.2 4.4 6.1 6.4 6.4 6.4 4.8

22
5.2
15 7 8 7 5 4 1 5 6 8 12
4.1 5.7 6.2 6.4 6.5 7.5 7.6 6.5 6.8 5.8 4.9

25 16 11 9 4 3 5 6 13
5.2 5.0 6.4 6.5 6.9 7.5 7.0 6.2 5.7
14.7 16.9 15.3 15.2 14.8 14.2 14.7 15.5 16.0

| | | | | | |
|---|---|---|---|---|---|
| | | 1016.66 | | | |
| 216+36 | | | 2.6 | 1014.1 | $\frac{13}{1.7}$ $\frac{9}{2.6}$ $\frac{6}{2.7}$ $\frac{.8}{1.3}$ |
| 216+40 | | | 4.5 | 1012.2 | $\frac{11}{2.3}$ $\frac{10}{2.9}$ $\frac{8}{2.9}$ $\frac{7}{4.4}$ $\frac{1}{2.6}$ $\frac{6}{2.8}$ $\frac{8}{1.5}$ |
| 216+52 | | | 3.3 | 1013.4 | $\frac{11}{2.6}$ $\frac{9}{3.3}$ $\frac{8}{4.6}$ $\frac{6}{5.1}$ $\frac{4}{4.4}$ $\frac{1}{4.0}$ $\frac{3}{3.6}$ $\frac{7}{3.0}$ $\frac{9}{1.5}$ |
| 216+63 | | | 3.9 | 1012.8 | $\frac{11}{3.1}$ $\frac{9}{4.1}$ $\frac{8}{4.3}$ $\frac{6}{4.0}$ $\frac{6}{3.5}$ $\frac{9}{2.4}$ $\frac{11}{1.0}$ |
| 217+00 | | | 5.3 | 1011.4 | $\frac{\frac{11}{2.6}}{14.1}$ $\frac{\frac{8}{5.0}}{11.7}$ $\frac{\frac{5}{5.1}}{11.6}$ $\frac{\frac{9}{4.8}}{11.9}$ $\frac{\frac{10}{3.7}}{13.0}$ |
| 217+15. | | | 6.2 | 1010.5 | $\frac{8}{4.1}$ $\frac{7}{5.3}$ $\frac{2}{5.6}$ $\frac{1}{6.0}$ $\frac{1}{5.8}$ $\frac{7}{5.6}$ $\frac{9}{5.8}$ $\frac{12}{3.2}$ |
| 217+25 | | | 6.9 | 1009.8 | $\frac{7}{4.0}$ $\frac{1}{5.7}$ $\frac{4}{6.6}$ $\frac{1}{7.1}$ $\frac{5}{6.8}$ $\frac{6}{6.0}$ $\frac{9}{6.0}$ $\frac{10}{6.2}$ $\frac{15}{3.4}$ |
| +28 | | | 7.1 | 1009.6 | $\frac{8}{4.0}$ $\frac{6}{5.4}$ $\frac{2}{5.9}$ $\frac{1}{6.8}$ $\frac{2}{7.5}$ $\frac{6}{6.8}$ $\frac{7}{6.0}$ $\frac{9}{6.3}$ $\frac{15}{3.8}$ |
| 217+47 | | | 6.5 | 1010.2 | $\frac{8}{4.9}$ $\frac{6-4}{6.2}$ $\frac{1}{7.0}$ $\frac{4}{7.1}$ $\frac{5}{6.8}$ $\frac{7}{6.7}$ $\frac{10}{7.1}$ $\frac{15}{4.7}$ |
| +50 | | | 6.6 | 1010.1 | $\frac{7}{5.0}$ $\frac{5}{6.4}$ $\frac{6}{7.0}$ $\frac{8}{6.8}$ $\frac{9}{7.3}$ $\frac{14}{4.7}$ |
| 218 | | | 8.2 | 1008.6 | $\frac{\frac{9}{7.0}}{09.7}$ $\frac{\frac{7}{7.8}}{08.9}$ $\frac{\frac{5}{7.9}}{08.8}$ $\frac{\frac{4}{8.1}}{08.6}$ $\frac{\frac{8}{8.0}}{08.7}$ $\frac{\frac{9}{8.2}}{08.5}$ $\frac{\frac{15}{5.4}}{11.3}$ |

| | | | | | |
|---|---|---|---|---|---|
| | | 1016.66 | | | |
| 218+28 | | | 9.5 | 1007.2 | |
| +30 | | | 11.6 | 1005.1 | |
| 218+50 | | | 12.2 | 1004.5 | |
| | 6.61 | 1011.70 | 11.57 | 1005.09 | |
| 218+66 | | | 5.2 | 1006.5 | |
| 218+70 | | | 5.5 | 1006.2 | |
| 219 | | | 6.1 | 1005.6 | |
| +50 | | | 7.6 | 1004.1 | |
| BM #29 | 4.47 | 1011.69 | 4.47 | 1007.23 | 1007.22 |
| 219+75 | | | 8.1 | 1003.6 | |
| 220 | | | 8.6 | 1003.1 | |
| | 4.54 | 1007.23 | 9.00 | 1002.69 | |

| | | | | |
|---|---|---|---|---|
| | 1007.23 | | | |
| 220+25 | | 4.6 | 1002.6 | |
| +50 | | 4.5 | 1002.4 | |
| +62 | | 4.6 | 1002.4 | |
| +70 | | 4.8 | 1002.4 | |
| 221 | | 5.8 | 1001.4 | |
| +50 | | 6.3 | 1000.9 | |
| +77 | | 6.7 | 1000.5 | |
| +80 | | 6.7 | 1000.5 | |
| +90 | | 7.3 | 999.9 | |
| 222 | | 7.5 | 999.7 | |

27/4.0 30/4.5

7/2.7 2/4.5 11/5.2 12/4.4 13-14/4.8 15/3.7 18/3.0 22/3.8

7/3.7 2/4.2 1/4.8 5/5.4 10/5.2 10.5-11/5.7 11-15/5.2 15/4.0

3/4.2 2/4.6 2/5.2-5.9 4/6.0-5.6 4/5.7 15/5.2 15.5/4.1

3/4.2 2/4.7 2/5.5 3/6.7 5/5.9 10/5.8 11/5.2 14/5.0 15/4.0

0.3 0.2.5 0.1.7 0.0.5 0.1.3 0.2.4 0.2.0 0.1.8 0.3.2

10/4.3 4/4.6 2/5.3 2/5.6 4/6.6 9/6.0 11/5.5 13/5.8 14/4.4

2.9 2.6 1.9 1.6 0.6 1.2 1.7 1.4 2.8

23/6.0 14/5.5 9/5.0 6/6.3 3/6.5 6/6.1-5.7 9/5.8 10/5.3 12/4.9

1.2 1.7 2.2 0.9 0.7 1.1 1.6 1.4 1.9 2.3

30 27 25/6.9 6.0 6.8 12/5.4 9/7.6 8/6.8 5/6.9 4/6.5 2/5.8 4/6.2 4-6/7.0 6.5/5.7

0.8 1.2 0.4 1.8 99.6 0.4 0.3 0.7 1.4 1.0 0.2 1.5

11/5.7 11/10.1 7/8.4-6.4 1/6.1 4/5.9 5.7/7.1 7/5.7

29/6.5

26/5.9 24/6.3 19/5.7 15/6.6 19/9.7 6/9.3 6-1/7.8 3/6.5 4/6.8 7/6.3

30/5.5

20 16/5.6 6.8 15/9.1 11/8.6 9/7.7 5/7.4 2/7.9 2/7.3 3/6.6

1.6 0.7 98.1 98.6 99.5 99.8 99.3 99.9 0.6

| | | | | |
|---|---|---|---|---|
| ✓ | | 1007.23 | | |
| 222+13 | | | 7.4 | 999.8 |
| | 3.05 | 1002.48 | 7.80 | 999.43 |
| ✓ +50 | | | 3.9 | 998.6 |
| ✓ +90 | | | 4.6 | 997.9 |
| ✓ 495 | | | 4.6 | 997.9 |
| ✓ 223 | | | 5.0 | 997.5 |
| ✓ +10 | | | 5.3 | 997.2 |
| ✓ +14 | | | 5.6 | 996.9 |
| | | | 5.02 | 997.18 |
| ✓ +38 | | | 6.9 | 995.6 |
| ✓ 56 | | | 7.9 | 994.6 |
| ✓ 224 | | | 9.0 | 993.5 |

30/6.6 27/6.3 18/7.4 11/7.4 7/8.4 2/7.9 1/7.0 4/6.6

30/3.1 16/3.0 11/3.7 8/3.5 6/4.1 2/4.2 3/3.2 7/2.6

17/4.6 11/5.9 8/5.2 5/5.8 2/5.0 6/3.6

23/4.8 18/4.7 10/5.8 9/8.1 8/9.2 3/8.7 2/5.1 6/3.9 7-9/4.4 10/3.0

21/5.0 17/5.1 14/6.3 10/7.1-5.3 5/9.4 2/8.1-5.3 6/4.3
97.5 97.4 96.2 95.4 94.2 93.1 94.4 97.2 98.2

18/5.5 16/6.5 10/6.8 10-7/8.1 3/7.1-5.9 4/5.0 7/5.3 9/3.6

18/5.5 15/7.2 7/7.4 5/6.1 4/5.3 6-7/5.5 8/4.0

17/5.4 15/6.1 13/9.1 9/9.3 6/8.7-7.7 3/6.5 4-6/6.9 7/5.2

15/6.4 13/8.1 9.5/8.3 9/9.1 7/9.2 5/8.5 6/7.9 7/4.7

17/6.8/95.7 14/8.8/93.7 10-8.9/93.6 10/10.9/92.5 4/10.1/92.4 4/7.8/94.7 11/6.9/95.6

| | | | | |
|---|---|---|---|---|
| | | 1002A8 | | |
| | 0.05 | 997.21 | 5.32 | 997.16 |
| 22A+30 | | | 4.5 | 992.7 |
| 225 | | | 5.2 | 992.0 |
| +50 | | | 6.5 | 990.7 |
| 226 | | | 7.8 | 989.4 |
| +22 | | | 9.5 | 987.7 |
| +50 | | | 8.9 | 988.4 |
| 227 | | | 10.4 | 986.8 |
| | 2.78 | 989.51 | 10.48 | 986.73 |
| +30 | | | 2.9 | 986.6 |
| +40 | | | 2.8 | 986.7 |

13 11 8-8 6 2 5 8 10 13
2.2 4.0 3.7-4.5 4.9 3.5 2.9 3.2 3.0 2.1

11 5 7 8-10 10
2.2 5.7 4.9 5.6 4.4
95.0 91.5 92.3 91.6 92.8

12 8 7 6 3 7 13
3.9 6.7 7.0 7.9 7.7 6.1-6.5 5.0

14 8 6 3 6 7-8 10
7.0 7.8-10.0 10.3 10.0- 8.4 7.7 7.1 7.9-7.3
90.2 89.4 87.2 86.9 87.2 88.8 89.5 90.1 89.3 89.9

12 10 8 4 1 1 5 7 8-10 11
2.3 7.6 10.7 10.6 9.2- 8.5 8.3 7.9 8.1 7.7
89.9 89.6 86.5 86.4 88.0 88.7 88.0 89.3 89.1 89.5

12 11-9 8 6 5 4 6 9
8.2 8.8 8.7 8.6 9.1 8.9 8.5 8.2

17 8 3 7 8 12
8.6 9.1 10.5 9.5 10.1 5.9
88.6 88.1 86.7 87.7 87.1 88.3

16 8 7 5 4 8 5
2.4 3.2 4.0 3.8 3.0 1.7 2.0

9 7 5 9 14 16
1.8-1.8 2.4 3.3-4.5 4.1 3.2

| | | | | | |
|---|---|---|---|---|---|
| | | 989.51 | | | |
| +48 | | 0 | 5.6 | 983.9 | |
| +56 | | | 5.4 | 984.1 | |
| 228 | | | 6.6 | 982.9 | |
| +19 | | | 6.8 | 982.7 | |
| +25 | | | 7.8 | 981.7 | |
| +50 | | | 7.0 | 982.5 | |
| +75 | | | 7.0 | 982.5 | |
| 229 | | | 7.5 | 982.0 | |
| 230 | | | 8.3 | 981.2 | |
| | 4.14 | 985.66 | 7.99 | 981.52 | |
| 230+98 | | | 5.6 | 980.1 | |

30/3.5 10/2.0 5/2.7 5/5.4 5/5.8 5/2.7 7/2.1

17/2.1 11/2.9 3/4.1 5/4.0 4/4.6 5/5.5 6/3.4 11/3.4

15/5.1/84.4 10/5.8/83.7 3/6.7/82.8 5/6.1/83.4 11/5.3/84.2

14/5.6 6/6.3 7/6.0

14/5.4 11/6.0 6/6.5 4/7.4 3/7.7 3/6.6 8/5.8

18/5.5 9/6.3 4/6.9 10/6.2

18/5.6/83.9 11/6.6/82.9 6/6.6/82.9 8/7.1/82.1 6/6.5/83.0 10/6.7/82.8 13/5.6/84.1 18/5.9/84.1 15/8.8/80.7

7/6.7/82.8 5/7.4/82.1 3/7.6/81.9 4/7.0/82.5

2/7.7/81.8 8/8.4/81.4 9/7.8/81.7

10/4.2/81.5 6/4.8/80.9 7/5.3/80.4 6/4.7/81.3

975.66
5.0

231 ✓ 6.3 979.4

231+16 ✓ 5.1 980.6

+20 ✓ 5.0 980.7

+28 ✓ 7.3 978.4

+40 8.3 977.4

+42 8.3 977.4

3.98 981.68 982.19

6/4.7 81.0 | 2/5.5 80.2 - 2/6.7 79.0 | 1/5.3 80.4 | 5/4.9 80.8 | 6/4.5 81.2

15.16/5.0 7.0 | 10/7.8 | 5/7.4 | 1/6.1 - 5.2 | 5/4.6 | 7/4.3

21/5.0 7.0 | 19/7.1 | 14/7.5 | 9/6.1 | 6/4.2 | 3/5.2

7/4.4 | 3/5.4 | 3/7.3 | 5/6.6 | 5/4.5

13/8.5 | 9/8.7 | 2/8.7 | 2/6.1 | 4/5.7 - 4.8

13/8.5 | 9/8.7 | 2/8.7 - 6.1 | 4/5.7 4.8

| | | | | | | |
|---|---|---|---|---|---|---|
| DM #32 | 4.18 | 977.41 | | | 973.23 | |
| 236 | | | | | | 6 / 4.8 |
| 235 | | | 3.2 | | | 4 / 3.0 |
| 234 | | | | | | 9 / 0.7 |
| | 9.21 | 985.95 | 0.67 | 976.74 | | |
| 233 | | | 7.6 | | | |
| 232 | | | 6.7 | | | |
| 231 +50 | | | 6.6 | | | |
| BM 31 | | | 4.17 | 981.78 | 982.19 | |

Aug. 20, 1931
R. Goodrich
S. Merritt
H. Barton
N. Chapman

## Rock Sections

| | | | | |
|---|---|---|---|---|
| Slope Stake | | | | |
| 66 - R. | 9.82 | 1166.03 | | 1156.21 |
| 66+50 | | | 10.8 | |
| 66+65 | | | 12.0 | |
| 72 | | | 12.6 | |
| | 8.65 | 1063.92 | 10.76 | 1055.27 |
| 79 | | | 11.1 | |
| 67 | | | 12.7 | |
| | | | 7.73 | 1156.19 1156.21 |



| | | | | | | | |
|---|---|---|---|---|---|---|---|
| | | (R) 14 | | | | | |
| 7 | 12 | | 16 | 22 | 28 | | |
| 10.7 | 11.5 | 9.9 | 6.0 | 3.8 | 3.0 | | |
| | | | | Ledge | | | 30 |
| | (R) | (R) | (R) | (R) | | | 2.7 |
| 10 | 13 | 15 | 15.2 | 16 | 20 | 26 | |
| 12.2 | 13.2 | 10.0 | 8.1 | 7.7 | 6.2 | 3.3 | |
| | | | Ledge | | | | |
| | (R) | (R) | (R) | | | | |
| 11 | 13 | 17 | 19 | 19.2 | 20 | 30 | |
| 12.9 | 13.4 | 11.8 | 9.2 | 7.3 | 6.1 | 2.7 | |
| | | | | Ledge | | | |
| | (R) | (R) | (R) | | | | |
| 10 | 13 | 14 | 16 | 17 | 30 | | |
| 11.3 | 12.0 | 11.1 | 9.9 | 7.6 | 0.6 | | |
| | | | | Top of Ledge | | | |
| | (R) | (R) | (R) | (R) | (R) | | |
| 5 | 13 | 18 | 21 | 25 | 28 | 28 | |
| 12.1 | 12.9 | 12.4 | 10.7 | 7.8 | 7.0 | 5.9 | |
| | | | | | | | 30 |
| | | | | | | | 4.3 |

over

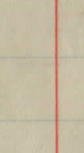
2+21

1+90 = E. end drive pipe

1+75 = ℄ drive way

1+62 - E. edge pond

1+50 = outlet pipe & W. end drive pipe
19" drive pipe




1+0

0+85

0+50

| | | HI | |
|---|---|---|---|
| B.M. | + 6.03 | 106.03 | 100.0 |
| 0+0 = W. line Herzer property | | | |
| | | HI | |
| B.M. | + 5.54 | 105.54 | |
| = S.W. ℄ S. head wall sta 2+21 | | | 100.0 |

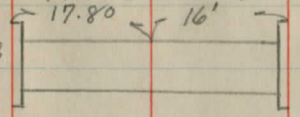
6-21-55

Profile & Ditch elev.

W. Wilson Mills Rd. ± 1500' W Chillicothe

72

Re: pond on Herzer lands




(97.43) FL. 8.6 drive pipe
25.6

(99.93) 6.1 / 12'

(99.73) 6.3 / 23

(99.93) 6.10

(100.03) 6.0

19' to edge $H_2O$ (100.83) 6.0 / 12'

26.5' → outlet pipe

(99.13) ditch 6.9 / 18

(100.93) 5.1

(100.93) 5.1 / 12'

(99.68) 6.35 / 21' water level at edge of water

(101.03) 5.0 / 18 no ditch

← 30' to edge $H_2O$

(101.93) 4.1

(100.83) 5.2 / 18 ditch

← ±100' to edge $H_2O$

(101.54) ditch 4.0 / 17'

103.24 2.3

(101.34) ditch 4.2 / 17'

N ℄ S

2+50

98.73
7.3

2+0

96.23
98
18'

99.38
6.65

95.53
10.5
25'

N

℄

S

4/10/56 Merritt Patterson ± Sta 189+87 to 203+00

Wilson Mills Rd HE + − ELEV.

Sta

Sta 198+26

BM A 5.51 1102.39 ~~105.51~~ 1096.88 ~~100.00~~

N Ditch | Road ℄ | S Ditch

X cut in NE4 N. Hdwl. Sta 198+26 Per Rd Plan

| | | | | | | |
|---|---|---|---|---|---|---|
| Sta 203 | | ℄ 1093.99 | 6.3 / 23 | 9.8 / 15 | 8.4 | 10.1 / 17 | 9.4 / 20 |
| 202+50 | | ℄ 1094.59 | 7.2 / 21 | 8.5 / 16 | 6.8 | 9.1 / 17 | 9.6 / 25 |
| 202+0 | | ℄ 1096.29 | 7.5 / 25 | 8.0 / 18 | 6.1 | 8.7 / 18 | 9.8 / 28 |
| 201+0 | | ℄ 1097.04 | 6.1 / 20 | 7.25 / 17 | 5.25 | 6.8 / 17 | 5.6 / 23 |
| 200+0 | | ℄ 1097.84 | 3.5 / 25 | 6.35 / 17 | 4.6 | 5.9 / 17 | 9.7 / 22 |
| Drive-N 199+66 | | ℄ 1097.79 | 3.5 / 32 | 3.5 / 26 | 6.7 / Ditch W. End Over 12" Conc Pipe | 9.7 / 17 | 4.6 | 5.6 / 18 | 4.2 / 22 |
| 199+0 | | ℄ 1096.59 | 5.4 / 30 Lawn | 5.2 / 20 | | 6.8 / 18 | 4.8 | 5.95 / 18 | 3.7 / 28 |
| ℄ Culvt 198+26 | | ℄ 1097.23 | 11.3 / 150 | 8.0 / 100 | 6.25 / 30 Lawn | 6.6 / 22 | 8.0 / 20 Ditch | 8.4 / 17.5 | 5.16 | 7.9 / 18 | 7.6 / 30 Swamp | 6.8 / 190 |

| Sta. | + | HI | − | ELEV. | Ditch N | Road ℄ | Ditch S |
|---|---|---|---|---|---|---|---|
| Drive N. | | ~~1105.57~~ | | | | | |
| 198+0 | | 1102.39 | | ℄1097.14 | 7.3 6.4 / 30 Garage | 5.25 | 7.3 / 17 — 5.8 / 23 — 6.7 / 30 |
| | | | | | 7.2 7.5 6.1 / Ditch W End — Ditch E End — ℄ Drive & Pipe 17 | | |
| Drive S. | | | | | | | |
| 197+45 | | | | ℄1096.99 | 5.0 / 60 House 4 — 5.5 / 30 Lawn — 6.2 / 16 | 5.4 | 5.6 / 18 ℄ Drive — 7.3 Ditch W. End — 5.5 / 30 |
| 197+0 | | | | ℄1096.79 | 6.5 / 60 House 4 — 6.8 / 30 Lawn — 6.5 / 17 | 5.6 | 7.3 / 18 — 4.3 / 24 |
| T.P. | 1.50 | 1098.09 | 5.80 | 1096.59 | | | |
| | | ~~101.21~~ | | ~~99.71~~ | | | |
| Drive S. | | | | | | | |
| 196+70 | | | | ℄1096.66 | 5.0 / 65 Lawn — 3.5 / 30 — 3.1 / 17 | 4.93 | 1.3 / 18 ℄ Drive — 3.1 Ditch W. End — .70 / 25 |
| 196+0 | | | | ℄1096.29 | 2.7 / 21 — 3.8 / 17 | 1.8 | 3.55 / 19 — 0.0 / 25 |
| 195+0 | | | | ℄1094.89 | 2.0 — 5.0 / 22 — 17 | 3.2 | 4.7 / 17 — 1.5 / 25 |
| 194+0 | | | | ℄1092.59 | 4.8 / 25 — 7.6 / 18 | 5.5 | 8.85 / 17 — 4.9 / 25 |
| Drive N. | | | | | | | |
| 193+05 | | | | ℄1088.59 | 10.3 / 75 — 9.05 / 30 — 12.8 W End Ditch — 8.4 / 18 ℄ Drive | 8.5 | 10.2 / 18 — 6.2 / 29 |
| 193+0 | | | | ℄1089.49 | Some | 8.6 | Some |

| | + | H.I. | − | ELEV. |
|---|---|---|---|---|
| Drive S. | | ~~1101.21~~ | | |
| | | 1098.09 | | |
| 192+20 | | | | ℄1087.19 |
| T.P. | 2.62 | 1089.52 ~~92.64~~ | 11.19 | 1086.90 ~~90.02~~ |
| 192+00 | | | | ℄1086.72 |
| ℄ Hillside culvt. | | | | |
| 191+62 | | | | ℄1087.52 |
| 191+00 | | | | ℄1085.02 |
| 189+87 | | | | ℄1084.49 |
| {189+87 | | | 5.13 | ~~87.51~~ |
| {B.M.B | (+ cut in NE ℄ S. Hdwl) | | | 1084.39 |
| T.P. | 10.11 | 1097.41 ~~100.53~~ | 2.22 | 1087.30 ~~90.42~~ |
| B.M. A | | | .53 | 1096.88 ~~100.00~~ |

| | | N Ditch | | Road ℄ | S Ditch | | |
|---|---|---|---|---|---|---|---|
| 13.5 / 60 | 12.3 / 30 | 11.4 / 22 | 12.8 / 18 | 10.9 | 11.1 / 17 ℄ Drive | 12.9 W End Pipe | 8.5 / 40 |
| | | 5.3 / 30 | 4.9 / 17 | 2.8 | 4.8 / 17 | 3.3 / 24 | |
| 11.2 / 150 | 9.9 / 100 | 9.0 / 75 | 8.4 / 20 Flow Line | 3.0 | 7.6 / 17 Inlet Flow Line | 3.4 / 21 | 2.8 / 25 |
| | | 8.8 / 75 | 7.6 / 20 | 4.5 | 6.3 / 17 | 6.9 / 30 | |
| 11.3 / 250 | 10.9 / 150 | 10.1 / 75 | 10.25 / 18 Flow Line N. | 5.03 | 10.1 / 17 Flow Line | 9.8 / 50 | 8.3 / 100 |

| | | | | |
|---|---|---|---|---|
| BM20 | 563 | 113.16 | | 112.753 |
| 156+15 | | | 6.6 | 26.6 |
| 155+50 | | | 6.0 | 27.2 |
| | 1182 | 114.293 | 20.5 | 1131.11 |
| 153+50 | | | 10.8 | 32.1 |
| | 888 | 115.162 | 0.19 | 114.274 |
| 155 | | | | |
| 155+50 | | | | |
| 156 | | | | |
| 152. | 2.5 | 1147 | | 114.2 |
| 152+50 | | | 6.0 | 114.07 |

&

28/80 24/81 13/77 12/81 9/75 3/68 5/62 13/67 16/75 22/79 24/108 29/106

19/0.1 16/2.2 7/55 4/6.2 2/58 3.5/60 6/56 12/54 22/59 30/70

−33/1.3 31/24 23/66 15/109 11/101 7.5/103 6/112 4/106 10/11.2 11/108 16/11.3 38/128

60/2.0 30/31 26.5/36 23/73

60/1.5 46/2.3 41/5.0 30/11.9

10:1 up 45/6.5 39/10.6 28/15.3

10:1+ 34/0.0 12/34 17.5/56 13.5/65 14/58 10.5/56 9/66 4/60 6/58 7/65 8/57 15/26 30/30

| | | | | |
|---|---|---|---|---|
| BM17 | 062 | 116954 | | 116892 |
| 145+70 | | | 4.3 | 1165.2 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 30 | 20 | 18 | 15 | 13 | 6 | 10 | 12 | 17 | 130 |
| 1.0 | 17 | 48 | 53 | 48 | 43 | 50 | 35 | 40 | 53 |

| | | |
|---|---|---|
| 145+273 | 240 | 116714 |
| 145+373 | 253 | 1167.01 |

24.3

14.3
0.7
15.6

66.52
0.89
65.63
7.0
1072.6
4.8
1068.6

8/1.5 6/2.8 1/2.6 | 7/4.4 8/2.9 10/2.9 11/2.3

11.4
5.3

7/2.0 3/3.2 | 2/4.2 6/4.1 8/3.5 11/3.7 16/5.0 30/3.1

PLEASE RETURN TO
GEAUGA COUNTY ENGINEER
COURT HOUSE
CHARDON, O.
PHONE 250-X

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 24 FEET WIDE. SIDE SLOPES 1½ to 1.

FOR SMALL BLACK EMBANKMENT.

| | 0 | .1 | .2 | .3 | .4 | .5 | .6 | .7 | .8 | .9 | |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 0 | 7.0 | 7.2 | 7.3 | 7.5 | 7.6 | 7.8 | 7.9 | 8.1 | 8.2 | 8.4 | 0 |
| 1 | 8.5 | 8.7 | 8.8 | 9.0 | 9.1 | 9.3 | 9.4 | 9.6 | 9.7 | 9.9 | 1 |
| 2 | 10.0 | 10.2 | 10.3 | 10.5 | 10.6 | 10.8 | 10.9 | 11.1 | 11.2 | 11.4 | 2 |
| 3 | 11.5 | 11.7 | 11.8 | 12.0 | 12.1 | 12.3 | 12.4 | 12.6 | 12.7 | 12.9 | 3 |
| 4 | 13.0 | 13.2 | 13.3 | 13.5 | 13.6 | 13.8 | 13.9 | 14.1 | 14.2 | 14.4 | 4 |
| 5 | 14.5 | 14.7 | 14.8 | 15.0 | 15.1 | 15.3 | 15.4 | 15.6 | 15.7 | 15.9 | 5 |
| 6 | 16.0 | 16.2 | 16.3 | 16.5 | 16.6 | 16.8 | 16.9 | 17.1 | 17.2 | 17.4 | 6 |
| 7 | 17.5 | 17.7 | 17.8 | 18.0 | 18.1 | 18.3 | 18.4 | 18.6 | 18.7 | 18.9 | 7 |
| 8 | 19.0 | 19.2 | 19.3 | 19.5 | 19.6 | 19.8 | 19.9 | 20.1 | 20.2 | 20.4 | 8 |
| 9 | 20.5 | 20.7 | 20.8 | 21.0 | 21.1 | 21.3 | 21.4 | 21.6 | 21.7 | 21.9 | 9 |
| 10 | 22.0 | 22.2 | 22.3 | 22.5 | 22.6 | 22.8 | 22.9 | 23.1 | 23.2 | 23.4 | 10 |
| 11 | 23.5 | 23.7 | 23.8 | 24.0 | 24.1 | 24.3 | 24.4 | 24.6 | 24.7 | 24.9 | 11 |
| 12 | 25.0 | 25.2 | 25.3 | 25.5 | 25.6 | 25.8 | 25.9 | 26.1 | 26.2 | 26.4 | 12 |
| 13 | 26.5 | 26.7 | 26.8 | 27.0 | 27.1 | 27.3 | 27.4 | 27.6 | 27.7 | 27.9 | 13 |
| 14 | 28.0 | 28.2 | 28.3 | 28.5 | 28.6 | 28.8 | 28.9 | 29.1 | 29.2 | 29.4 | 14 |
| 15 | 29.5 | 29.7 | 29.8 | 30.0 | 30.1 | 30.3 | 30.4 | 30.6 | 30.7 | 30.9 | 15 |
| 16 | 31.0 | 31.2 | 31.3 | 31.5 | 31.6 | 31.8 | 31.9 | 32.1 | 32.2 | 32.4 | 16 |
| 17 | 32.5 | 32.7 | 32.8 | 33.0 | 33.1 | 33.3 | 33.4 | 33.6 | 33.7 | 33.9 | 17 |
| 18 | 34.0 | 34.2 | 34.3 | 34.5 | 34.6 | 34.8 | 34.9 | 35.1 | 35.2 | 35.4 | 18 |
| 19 | 35.5 | 35.7 | 35.8 | 36.0 | 36.1 | 36.3 | 36.4 | 36.6 | 36.7 | 36.9 | 19 |
| 20 | 37.0 | 37.2 | 37.3 | 37.5 | 37.6 | 37.8 | 37.9 | 38.1 | 38.2 | 38.4 | 20 |
| 21 | 38.5 | 38.7 | 38.8 | 39.0 | 39.1 | 39.3 | 39.4 | 39.6 | 39.7 | 39.9 | 21 |
| 22 | 40.0 | 40.2 | 40.3 | 40.5 | 40.6 | 40.8 | 40.9 | 41.1 | 41.2 | 41.4 | 22 |
| 23 | 41.5 | 41.7 | 41.8 | 42.0 | 42.1 | 42.3 | 42.4 | 42.6 | 42.7 | 42.9 | 23 |
| 24 | 43.0 | 43.2 | 43.3 | 43.5 | 43.6 | 43.8 | 43.9 | 44.1 | 44.2 | 44.4 | 24 |
| 25 | 44.5 | 44.7 | 44.8 | 45.0 | 45.1 | 45.3 | 45.4 | 45.6 | 45.7 | 45.9 | 25 |
| 26 | 46.0 | 46.2 | 46.3 | 46.5 | 46.6 | 46.8 | 46.9 | 47.1 | 47.2 | 47.4 | 26 |
| 27 | 47.5 | 47.7 | 47.8 | 48.0 | 48.1 | 48.3 | 48.4 | 48.6 | 48.7 | 48.9 | 27 |
| 28 | 49.0 | 49.2 | 49.3 | 49.5 | 49.6 | 49.8 | 49.9 | 50.1 | 50.2 | 50.4 | 28 |
| 29 | 50.5 | 50.7 | 50.8 | 51.0 | 51.1 | 51.3 | 51.4 | 51.6 | 51.7 | 51.9 | 29 |
| 30 | 52.0 | 52.2 | 52.3 | 52.5 | 52.6 | 52.8 | 52.9 | 53.1 | 53.2 | 53.4 | 30 |
| 31 | 53.5 | 53.7 | 53.8 | 54.0 | 54.1 | 54.3 | 54.4 | 54.6 | 54.7 | 54.9 | 31 |
| 32 | 55.0 | 55.2 | 55.3 | 55.5 | 55.6 | 55.8 | 55.9 | 56.1 | 56.2 | 56.4 | 32 |
| 33 | 56.5 | 56.7 | 56.8 | 57.0 | 57.1 | 57.3 | 57.4 | 57.6 | 57.7 | 57.9 | 33 |
| 34 | 58.0 | 58.2 | 58.3 | 58.5 | 58.6 | 58.8 | 58.9 | 59.1 | 59.2 | 59.4 | 34 |
| 35 | 59.5 | 59.7 | 59.8 | 60.0 | 60.1 | 60.3 | 60.4 | 60.6 | 60.7 | 60.9 | 35 |
| 36 | 61.0 | 61.2 | 61.3 | 61.5 | 61.6 | 61.8 | 61.9 | 62.1 | 62.2 | 62.4 | 36 |

Calculated by Julien A. Hall, M. Am. Soc. C. E.

MADE IN GERMANY.

R.